Senior Center Town of Sturbridge

STORMWATER MANAGEMENT PLAN, EROSION AND SEDIMENTATION CONTROL PLAN, AND LONG TERM OPERATIONS AND MAINTENANCE PLAN

March, 2023



Prepared by: With Waterfield Design Group 50 Cross Street | Winchester, Massachusetts | 01890 | t 781.756.0001 f 781.756.0007

WDG Project No.: 1717

Introduction:

This Stormwater Management Plan, Erosion and Sedimentation Control Plan and Long Term Operations and Maintenance Plan has been prepared in conformance with the requirements of the Stormwater Management Regulations of the Town of Sturbridge and the Site Plan Review criteria of the Town of Sturbridge Planning Board. The project is within the Sturbridge Groundwater Overlay Protection District and meets the requirements of Groundwater Protection District Bylaw.

Name and Address of Applicant/Owner/Contact:

Town of Sturbridge Senior Center Robyn Chrabascz, Facilities Manager 308 Main Street Sturbridge, MA 01566 Phone: 774-304-1408

Site Description:

The subject parcel is approximately 1.79+/- acres in size and located at 480 Main Street in Sturbridge. The parcel is abutted by the 4 Arnold Road, a residential property to the north, a hotel to the east, by Main Street (Route 20) to the south and Arnold Road to the west and south. An existing 3,089 SF Senior Center is on the lot with associated parking and walking paths.

The site is the existing building, paved parking, lawn, and woods. The overall site gradient slopes from the north to the south. The woods have a drainage channel that directs runoff to Main Street. The existing building and paved parking sheet flow to the lawn area south of the building and then onto Main Street.

Description of Proposed Project/Proposed Land Use:

The applicant is proposing to construct an addition to the existing building and increases in associated parking. Water and sewer will be supplied through existing mains in Arnold Road. Electricity will be supplied through existing utilities. No gas is proposed on site. The site is zoned Commercial Tourist.

Existing Conditions:

The site is a developed area with a building, paved parking, lawn, and woods.

Proposed Conditions:

The applicant is proposing to construct an addition to the existing building and increase the parking to provide for the increased capacity of the building. Stormwater drainage for the proposed site will collect in deep sump catch basins which will be directed to proprietary separators and then outlet to underground infiltration chambers. The chambers will have overflow pips outleting to the existing wooded swale on site.

Low Impact Development (LID) Practices

The Town of Sturbridge Stormwater Management Regulations require LID measures be considered to the maximum extent feasible. The DEP Stormwater checklist requires that the proponent document which environmentally sensitive and LID Techniques were considered during the planning and design of the projects.

Below are a list of environmentally sensitive and LID Techniques and how they were or were not able to be implemented into the project:

No disturbance to any Wetland Resource Areas

The proposed project is the redevelopment of an existing site. The project does not disturb any resource areas.

Site Design Practices

The site is designed to incorporate the minimum amount of facilities necessary in order for the project to be financially viable. Wherever practical the design was limited to decrease disturbance.

Minimize Disturbance to Existing Trees and Shrubs

The applicant has sought to minimize the disturbance of existing trees and shrubs wherever possible. The wooded area outside of the proposed grading necessary for the site will be maintained.

Use of "country drainage" versus curb and gutter conveyance and pipe/vegetated filter strips

Give the high-performance needs of the paved parking and walking areas on the site and the need to maximize the parking areas the use of "county drainage" was not practical.

Bioretention Area

Give the high-performance needs of the paved parking and walking areas on the site and the need to maximize the parking areas the use of bioretention areas was not practical.

Constructed Wetlands

The site is designed to be a Senior Center to be used elderly adults. Constructed wetlands could breed mosquitos and unnecessarily bring these disease carrying insects into contact with the Center's users.

Treebox Filter

Give the high-performance needs of the paved parking and walking areas on the site, the need to maximize the parking areas, and the large volume of runff created by the impervious area on site treebox filters were not practical to use on site.

Water Quality Swales & Grass Channels

Give the high-performance needs of the paved parking and walking areas on the site and the need to maximize the parking areas the use of water quality, and grass swales was not practical.

Green Roof

The maintenance and additional structural construction necessary to install and maintain a green roof on the proposed building is not economically feasible for the Town.

Permeable Pavements

Give the high-performance needs of the paved parking and walking areas on the site, the need to maximize the parking areas and the need of the high vehicle trip loadings of the parking areas the use of permeable pavers was not possible.

Cisterns

Cistern and water reuse are not financially viable systems to incorporate into the site design for the Town of Sturbridge constructing and operating the site.

Identify & Map Critical Environmental Resources

There are no critical environmental resources on the site.

Delineate Building to Avoid Environmental Resources & Appropriate Buffers The building has been located on the site to avoid environmental resources and appropriate buffers.

Develop Methods to Minimize Impervious Surfaces and Preserve Open Space.

The parking, access drives, and walkways have been minimized to provide impervious area for the what is needed to access and park at the site only. In addition, the wooded open space in the east of the property have been preserved outside of the grading area for the site improvements.

Stormwater Credits

The proposed project is not seeking any Stormwater Credits.

Total Site Area

Total Site Area to be Developed = 1.45 acres

Existing Impervious Area = 0.48 acres

Proposed Impervious Area = 0.92 acres

Soils

According to the NRCS Custom Soil Resource Report, the soils on site are listed as 420B - Canton fine sandy loam.

Canton is a well-draining soil with gentle to moderate slopes.

Test pits conducted at the site found fine sandy loams in the naturally occurring layers of in the test pits. Ground water or refusal due to ledge or boulders was found 3' to 8' below grade.

100 Year Floodplain

No portion of the site is within the 100' Year Floodplain.

Standard 1: No New Untreated Discharges

The new development areas on the site will flow overland and enter deep sump catch basins, proprietary separators, and underground infiltration chambers with overflows to the existing wooded swales which discharge to the Town drainage system in Main Street.

Since the runoff from the developed impervious surfaces on the site will be treated in accordance with the requirements of the Stormwater Management Regulations of the Town of Sturbridge and since the discharge will flow to the existing Town drainage system which currently accepts site runoff, no new untreated discharge will be added to the site. Therefore, Standard 1 has been met by the proposed project.

Standard 2: Peak Rate & Volume Attenuation

The proposed project involves the development of a predominantly developed site. Attached to this report are the existing and proposed (site developed) runoff calculations for the Project for the 2, 10, and 100 year storms.

All calculations were prepared using SCS Methods consistent with the requirements of the Wetland Protection Regulations and the 2008 MADEP Stormwater Handbook. The calculations were prepared using HydroCAD version 10.00 by Applied Microcomputers Systems. Soils data for the modeling was obtained from the National Resource Conservation Service Soil Map (Online) for the Town of Sturbridge (see attached Existing Watershed Plans and copy of a portion of the Map covering the site area) and field test pits (see attached Test Pit Soil Logs). Ground cover data is based on existing and proposed site conditions, aerial maps, and times of concentration are based on the tributary watershed characteristics. Hydrologic soil group data was obtained from the SCS National Engineering Handbook NEH #4 - Hydrology. Times of concentration for the study were computed using SCS Methodology. Rainfall data for the study is based on NRCC Extreme Precipitation Tables.

	Discharge Poir	nt #1		Discharge Poir	nt #1
Storm	Existing Peak	Proposed	Storm	Existing	Proposed
Return	Inflow Rate	(Site	Return	Volume of	(Site
Period	(c.f.s.)	Developed)	Period	Runoff (af)	Developed)
(years)	× /	Peak Inflow	(years)		Volume of
0,		Rate (c.f.s.)			Runoff (af)
2	1.94	0.39 (-1.55)	2	0.298	0.099 (-0.199)
10	4.12	2.75 (-1.37)	10	0.648	0.310 (-0.338)
100	10.04	9.88 (-0.16)	100	1.649	1.119 (-0.530)
100	10.04		100	1.649	1.119 (-0.53

Based on the results of the calculations as demonstrated above, the requirements of Standard 2 have been met and the redevelopment of the site will not result in any net increase in the peak rate of runoff or the runoff volume from the site.

Standard 3: Recharge

The soils at the site are Hydrologic Soil Group Class B soils.

See the infiltration calculations attached to the end of the report for the stormwater infiltration calculations.

Infiltration rates used are from the Rawls rates chart in the 2008 MADEP Stormwater Handbook.

As the infiltration calculations show, the proposed design provides the required recharge volume of the Stormwater Management Regulations of the Town of Sturbridge. Therefore, Standard 3 has been met by the proposed project.

Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)

Does not apply to the site.

Standard 6: Critical Areas

Does not apply to the site.

Retain volume of 1" of runoff

The proposed infiltration units retain the volume of runoff equivalent to, or greater than, one inch multiplied by the total postconstruction impervious surface area on the site.

See attached calculations.

Therefore, this item has been met.

Remove 80% TSS and 60% TP

The proposed project removes 80% of the average annual load of total suspended solids (TSS) generated from the total postconstruction impervious area on the site, see attached TSS removal calculations and 60-70% of the average annual load of total phosphorus (TP) generated from the total post-construction impervious surface area on the site, per the MA DEP Handbook for Infiltration Basins.

The Contech Units act as Oil/Grease Separators to meet the requirements of the Groundwater Protection Overlay District.

Therefore, this item has been met.

Standard 8: Construction Period Pollution Prevention Plan/Erosion and Sedimentation Control Plan

Erosion Control and Construction Sequencing

With regard to work proposed on the project and erosion and siltation control, the sequence of activities will generally take place as follows:

- 1. Prior to general gravel roadway removal, clearing, grubbing or topsoil stripping, place all strawbales, silt fence, and erosion control dikes in the location shown on the drawings. Although installation of these measures can be phased according to the construction schedule, strawbales, silt fence, and erosion control dikes must be in place prior to any work in a specific location.
- 2. Prior to any earthwork operations, install temporary siltation sump/filtration dams and swales with check dams and truck tracking pad in the locations approved by the Landscape Architect. These measures may be installed in phases according to the construction schedule, but must be completed prior to earthwork operations in the adjacent work area.
- 3. Damaged or loose strawbales and silt fence shall be replaced as necessary to maintain their function of controlling erosion and siltation. Damaged or broken down check dams and filtration dams shall be replaced immediately. Truck tracking pad shall be replaced as necessary to maintain its function of controlling erosion and siltation to the work area.
- 4. Remove any accumulation of silt or soil build-up behind strawbales, silt fence, check dams, and filtration dams as it occurs. Remove accumulations of silt and soil build-up from the siltation sumps and silt traps when it is approximately 18 inches deep. Replace the gravel filter on the inside of the filtration dams when it becomes clogged with silt or does not permit free drainage of stormwater through it, whichever occurs first.
- 5. Throughout excavation, filling, and grading operations, in addition to drainage swales, check dams, siltation sumps/filtration dams, and other items shown on the drawings, the Contractor shall take other necessary precautions, including installation of temporary drainage swales, siltation sumps/filtration dams, check dams, strawbales, silt fences, and temporary pipe, to direct and control drainage from disturbed areas on the site so that erosion and siltation is minimal. In addition, no erosion or discharge of silt or larger particles shall occur in areas to remain undisturbed or onto adjacent properties.
- 6. Remove all erosion control measures, including strawbales, silt fence, siltation sumps and check dams, only when construction is completed, upland surfaces are stabilized and the piped drainage system is fully operational and it has been approved to do so.

If the Contractor anticipates deviations from the above procedures, he shall obtain written approval from the Engineer prior to proceeding.

Erosion and Sediment Control BMP's

The Erosion and Sediment Controls represent the suggested best management practices proposed for the project. The Contractor's approach to controlling stormwater runoff from the site may vary somewhat; however they must update the SWPPP for the project to reflect the changes and implement appropriate corresponding erosion control measures.

The use of erosion and sediment controls are mandatory and must be employed to minimize impacts to adjacent areas during construction. If sediment escapes the construction site, off-site accumulations of sediment must be removed at a frequency sufficient to minimize off-site impacts.

The control practices which are required to minimize stormwater pollution during construction must remain functional until disturbed areas have been stabilized. Erosion control products are to be installed and maintained in accordance with manufacturer's specifications and good engineering practices.

The most important aspects of controlling erosion and sedimentation are limiting the extent of drainage structures. These fundamental principles will be the key factors in the contractor's control of erosion on the project site. If appropriate, the

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contractor will construct temporary diversion swales and settling basins or use a settling tank. If additional drainage or erosion control measures are needed, they will be located up-gradient from the hay bales and silt fences.

The contractor is responsible for the maintenance and repair of all erosion control devices on-site. All erosion control devices will be regularly inspected. At no time will silt-laden water be allowed to enter sensitive areas (wetlands, streams, and drainage systems). Any runoff from disturbed surfaces will be directed through a sedimentation process prior to being discharged to the existing on site drainage system.

The contractor will establish a staging area on a lot to be disturbed, outside the wetlands buffer zone for the overnight storage of equipment and stockpiling of materials.

In the staging area, the contractor will have a stockpile of materials required to control erosion on-site to be used to supplement or repair erosion control devices. These materials will include, but are not limited to hay bales, silt fence, erosion control matting, and crushed stone. As mentioned previously, erosion and sedimentation controls will be employed to minimize the erosion and transport of sediment into resource areas during the earthwork and construction phases of the Project. Erosion and sedimentation control measures will be installed prior to site excavation or disturbance and will be maintained throughout the construction period.

The contractor is responsible for erosion control on the site and will utilize supplemental erosion control measures to supplement the erosion controls shown on the plans prepared for this project to work with his day to day operations at the site.

Primary erosion control techniques proposed include hay bale barriers, silt fence barriers, inlet sediment traps, siltation control dikes, a stabilized construction entrance, temporary diversion channels, and temporary sedimentation ponds when applicable. A detailed description of each technique is discussed below. During the growing season, slope stabilization will be achieved by applying topsoil followed by seeding and mulching as soon as final grades are achieved. Organic mulching, jute netting, geotextiles, or a combination will be used to stabilize slopes completed outside of the growing season.

Best Management Practices (BMPs)

Silt Fence Strawbale Barriers

Erosion control barriers (silt fences or strawbale dike) will be installed prior to the start of construction. These barriers will remain in place until all tributary surfaces have been fully stabilized.

Strawbale barriers will be placed to trap sediment transported by runoff before it reaches the drainage system or leaves the construction site. In areas where high runoff velocities or high sediment loads are expected, silt fencing may be installed adjacent to the strawbale barriers. This semi-permeable barrier made of a synthetic porous fabric will provide additional protection. The silt fences and hay bale barrier will be replaced as determined by periodic field inspection. The underside of hay bales will be kept in close contact with the earth and reset as necessary. Hay bale barriers and siltation fences will be maintained and cleaned until slopes have healthy stands of grass.

Diversion Channels

Diversion channels may be used to intercept and divert runoff from slopes that are exposed during construction. These diversions will minimize the development of concentrated runoff down slopes, which could produce gully erosion. Diversions will also be used to collect runoff from construction areas and convey it to temporary sediment basins or traps. Temporary diversions will remain in place until slopes are stabilized or graded level. If vegetation of the diversion channel is required to avoid erosion of the channel, the channel will be temporarily stabilized to ensure viability of the grass seed.

Temporary Sediment Ponds

Temporary sediment ponds/basins will be constructed as necessary on the site either as excavations or bermed water detention structures, depending on grading. These temporary ponds will retain runoff for a sufficient period of time to allow suspended soil particles to settle out prior to discharge. These temporary basins will be located at low points on the site and will receive runoff from temporary diversion swales. Discharge points from sediment basins will be stabilized as necessary to minimize

erosion. The bottom of sediment basins will be cleaned periodically, with the sediment removed to a secure location to prevent siltation of natural waterways.

Utility Construction

The Contractor will construct utility trenches in a manner that will not direct runoff toward drainage system structures.

Stabilization Activities

All disturbed surfaces will be stabilized within 14 days after construction in any portion of the project site is completed or is temporarily halted, unless additional construction is intended to be initiated within 14 days. The Contractor will not disturb more area than can be stabilized within 14 days unless the area is to remain active. The Contractor will not disturb more area than can be stabilized within the same construction season.

Slope Stabilization

The smallest practicable area of land will be exposed at a time. Slopes greater than three-to-one (horizontal to vertical) will be stabilized with seed, organic mulch, jute fabric, or rip-rap, as appropriate, to prevent erosion during construction. After disturbed areas have been stabilized, the temporary erosion control measures will be removed and accumulated sediment will be removed and disposed of in an appropriate location. Disturbed areas will be stabilized with appropriate ground cover as soon as possible. After the removal of temporary erosion control measures, disturbed areas will receive a layer of topsoil for stabilization.

Stabilized Construction Entrance

Temporary stabilized construction entrances will be installed at the project site. The purpose of the construction entrance is to remove sediment attached to vehicle tires and to minimize sediment transport and deposition onto public road surfaces. The construction entrances will be composed of beds of crushed stone which will be replenished as necessary to maintain their proper function.

Inspections

The 2022 EPA Construction General Permit Conditions require routine inspections of the site and careful documentation of events and conditions. The following inspection activities will be completed by a qualified, designated site monitor.

- Erosion control, sedimentation prevention, and stormwater management measures will be inspected at least once per week throughout the construction period.
- All controls, outfalls, and potential problem areas will also be inspected within 24 hours of any storm exceeding 0.5 inches of precipitation.

A log of inspection results will be maintained on-site and will include the name of the inspector, date, major observations, and necessary corrective measures.

Built up sediment will be removed when it has reached one-third the height of the silt fence.

All needed repairs or modifications will be reported to the contractors to permit the timely implementation of required actions. Where necessary repairs do not pose an immediate concern, repairs or modifications will be implemented within two (2) days of inspection.

The SWPPP for the project will be modified within seven days to reflect any modifications to measures as a result of inspection.

A report summarizing the scope of the inspection, name(s) and qualifications of personnel making the inspection, the date(s) of the inspection, major observations relating to the implementation of the SWPPP, and actions taken will be made and retained as part of the SWPPP for at least three years after the date of the inspection.

Weekly reports of maintenance and inspection activities will be maintained on-site, in conformance with the NPDES permit conditions.

Maintenance

The following maintenance practices will be used by the Contractor to maintain erosion and sediment controls. Maintenance activities will be documented on the Inspection Report Forms.

Erosion and sediment control measures and other protective measures must be maintained in effective operating condition.

- If site inspections indicate that BMPs are not operating effectively, maintenance must be performed as soon as possible and before the next storm event whenever practicable to maintain the continued effectiveness of the BMPs. If implementation before the next storm event is impracticable, the situation must be documented in the SWPPP and alternative BMPs must be implemented as soon as possible.
- If existing BMPs need to be modified or if additional BMPs are necessary for any reason, implementation must be completed before next storm event whenever practicable. If implementation before the next storm event is impracticable, the situation must be documented in the SWPPP and alternative BMPs must be implemented as soon as possible.
- Pollution prevention measures must be maintained in good working order. If a repair is necessary, it will be initiated, if practicable, within 24 hours of report.
- Accumulated sediment within the catch basin inlet protection must be removed on a weekly basis.
- Maintenance and inspection of pollution prevention measures must be continued on the site for as long as a portion of the site remains disturbed.
- Stabilization measures will be initiated as soon as practicable on portions of the site where construction has temporarily or permanently ceased. This will occur in NO CASE more than 14 days after construction activities have temporarily or permanently ceased.
- If issues are identified at hazardous materials storage areas, corrective actions will be implemented immediately. If leaks or spills are identified procedures outlined in Standard 9 will be followed.

Record Keeping

Records will be retained for a minimum period of at least 3 years after the permit is terminated. Any time the following activities occur the *Grading and Stabilization Activities Log* will be filled out:

- When major grading activities occur
- When construction activities temporarily or permanently cease on a portion of the site
- When an area is either temporarily or permanently stabilized

Log of Changes To The SWPPP

This SWPPP must be modified as necessary to:

- Ensure permit compliance when notified by EPA that the plan does comply
- Include additional or modified BMPs that correct problems identified as a result of an inspection. Revisions must be completed with seven (7) calendar days following the inspection.

- Ensure the effectiveness of the SWPPP in eliminating or significantly minimizing pollutants from stormwater discharges from the site.
- Prevent the reoccurrence of release of a hazardous material or oil.
- Address a change in design, construction, operation, or maintenance which has or may have a significant effect on the potential for the discharge of pollutants.

All modifications to the SWPPP must be recorded on the SWPPP Amendment Log included in the SWPPP Appendix.

Stockpiling

All materials to be stockpiled on site shall be stockpiled outside of the 100 year floodplain in the area of the proposed building.

Hazardous Materials

No hazardous materials are located on the site.

Training

Training sessions must be provided by the Contractor for construction personnel. The training will review specific BMPs used in the work are as well as reporting and response measures that may be needed by either construction personnel and/or inspectors to implement the SWPPP. Additionally, appropriate construction personnel will be trained in the operation and maintenance of equipment to prevent the discharge of oil/hazmat and spill response procedures. Training sessions will highlight known spills or releases and recently developed precautionary measures. The Training Log shall be kept up to date by the Contractor.

69 Route 84, Sturbridge MA

Report No.	
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Stormwater Construction Site Inspection Report

General Information				
Project Name	Sturbridge Senio	or Center		
NPDES Tracking No.		Location		480 Main Street
Date of Inspection		Time	Start/End	Sturbridge, MA
Date of hispection		TIME	Start/Enu	
Inspector's Name(s) & Title				
Inspector's Company				
Inspector's Contact Information				
Inspector's Qualifications				
Describe present				
phase of construction				
construction				
Type of Inspection: Regular Pre-s	storm event 🛛 🗖 De	uring storm event	Post-	storm event
		Weather Inform	nation	
Has there been a storn	n event since the last	inspection?	Yes ⊒No	
If yes, provide: Storm Start Date & Time	e: Storm Dura	tion (hrs):	Approximate A	Amount of Precipitation (in):
Weather at time of this				
□ Clear □Cloudy □ Rain □ Sleet □ Fog □ Snowing □ High Winds □ Other: Temperature:				
Have any discharges occurred since the last inspection? If yes, describe:				
Are there any discharges at the time of inspection? □Yes □No If yes, describe:				

Site-specific BMPs

ВМР	BMP Installed?	BMP Maintenance Required?	Corrective Action Needed and Notes
Hay Bales / Silt Fence	□Yes □No	□Yes □No	
Catch Basin Protection	□Yes □No	□Yes □No	
Interior Site Erosion Controls	□Yes □No	□Yes □No	
Temporary Check Dams	□Yes □No	□Yes □No	
Diversion Channels	□Yes □No	□Yes □No	
Temporary Sediment Basins	□Yes □No	□Yes □No	
Stabilized Construction Entrance	□Yes □No	□Yes □No	
Street Sweeping / Construction Access	□Yes □No	□Yes □No	
Temp. and Permanent Slope Stabilization	□Yes □No	□Yes □No	
Dust Control	□Yes □No	□Yes □No	

N/A – Not Applicable

Overall Site Issues

BMP/activity	Implemented?	Maintenance Required?	Corrective Action Needed and Notes
Are all slopes and disturbed areas not actively being worked properly stabilized?	□Yes □No	□Yes □No	
Are natural resource areas (e.g., streams, wetlands, mature trees, etc.) protected with barriers or similar BMPs	□Yes □No	□Yes □No	

BMP/activity	Implemented?	Maintenance Required?	Corrective Action Needed and Notes
Are perimeter controls and sediment barriers adequately installed (keyed into substrate) and maintained?	□Yes □No	□Yes □No	
Are discharge points and receiving waters free of any sediment deposits?	□Yes □No	□Yes □No	
Are storm drain inlets properly protected?	□Yes □No	□Yes □No	
Is the construction exit preventing sediment from being tracked into the street?	□Yes □No	□Yes □No	
Is trash/litter from work areas collected and placed in covered dumpsters?	□Yes □No	□Yes □No	
Are washout facilities (e.g., paint, stucco, concrete) available, clearly marked, and maintained?	□Yes □No	□Yes □No	
Are vehicle and equipment fueling, cleaning, and maintenance areas free of spills, leaks, or any other deleterious material?	□Yes □No	□Yes □No	
Are materials that are potential stormwater contaminants stored inside or under cover?	□Yes □No	□Yes □No	
Are non-stormwater discharges (e.g., wash water, dewatering) properly controlled?	□Yes □No	□Yes □No	

BMP/activity	Implemented?	Maintenance Required?	Corrective Action Needed and Notes
(Other)	□Yes □No	□Yes □No	

In the event of a spill refer to the Spill Response Procedure and contact appropriate agencies. Refer to SWPPP for Spill Prevention Plan and Response Procedures.

Are sediment / pollution discharges from the site present?

Describe any corrective action at this time:

Non-Compliance

Describe any incidents of non-compliance not described above:

General Comments (Attached figures to show locations of concern):

Are Additional Erosion Control Measures Needed?

□ No □ Yes	If yes, describe:	
Notes:		

CERTIFICATION STATEMENT

"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations."

Print name and title:

Signature: _____

Date: _____

** A copy of this report should be placed in the Monitoring Section of the Stormwater Pollution Prevention Plan.

Corrective Action Log

Project Name: Sturbridge Senior Center SWPPP Contact:

Inspection Date	Inspector Name(s)	Description of BMP Deficiency	Corrective Action Needed (including planned date/responsible person)	Date Action Taken/ Responsible person

SWPPP Amendment Log

Project Name: Sturbridge Senior Center SWPPP Contact:

Amendment No.	Description of the Amendment	Date of Amendment	Amendment Prepared by [Name(s) and Title]

Subcontractor Certifications/Agreements

SUBCONTRACTOR CERTIFICATION STORMWATER POLLUTION PREVENTION PLAN

Project Number: _____

Project Title: Sturbridge Senior Center

Operator(s):

As a subcontractor, you are required to comply with the Stormwater Pollution Prevention Plan (SWPPP) for any work that you perform on-site. Any person or group who violates any condition of the SWPPP may be subject to substantial penalties or loss of contract. You are encouraged to advise each of your employees working on this project of the requirements of the SWPPP. A copy of the SWPPP is available for your review at the office trailer.

Each subcontractor engaged in activities at the construction site that could impact stormwater must be identified and sign the following certification statement:

I certify under the penalty of law that I have read and understand the terms and conditions of the SWPPP for the above designated project and agree to follow the BMPs and practices described in the SWPPP.

This certification is hereby signed in reference to the above named project:

Company: _____

Address: _____

Telephone Number: _____

Type of construction service to be provided:

Signature:

Title: _____ Date: _____

Grading and Stabilization Activities Log

Project Name: Sturbridge Senior Center SWPPP Contact:

Date Grading Activity Initiated	Description of Grading Activity	Date Grading Activity Ceased (Indicate Temporary or Permanent)	Date When Stabilization Measures are Initiated	Description of Stabilization Measure and Location

SWPPP Training Log

Stormwater Pollution Prevention Training Log

Project Nam	ie:					
Project Loca	Project Location:					
Instructor's I	nstructor's Name(s):					
Instructor's	Title(s):					
Course Loca	ation:			Date:		
Course Len	gth (hours):					
Stormwater	Training Topic: (c	heck	k as appropriate)			
Erosion	Control BMPs		Emergency Proce	dures		
Sedime BMPs	nt Control		Good Housekeepi	ing BMPs		
Non-Sto	ormwater BMPs					
Specific Tra	ining Objective:					

Attendee Roster: (attach additional pages as necessary)

No.	Name of Attendee	Company
1		
2		
3		
4		
5		
6		
7		
8		
9		

Delegation of Authority Form

Delegation of Authority

I, _____ (name), hereby designate the person or specifically described position below to be a duly authorized representative for the purpose of overseeing compliance with environmental requirements, including the Construction General Permit, at the construction site. The designee is authorized to

sign any reports, stormwater pollution prevention plans and all other documents required by the permit.

 (name of person or position)
 (company)
(address)
(city, state, zip)
(phone)

By signing this authorization, I confirm that I meet the requirements to make such a designation as set forth in ______ (Reference State Permit), and that the designee above meets the definition of a "duly authorized representative" as set forth in ______ (Reference State Permit).

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Name:	
Company:	
Title:	
Signature:	
Date:	

Standard 9: Long Term Operation and Maintenance Plan

An Operation and Maintenance Plan is summarized below and will be incorporated into the construction documents for this project.

In accordance with the Stormwater Management Policy issued by the Department of Environmental Protection (DEP), Waterfield Design Group, Inc. has prepared the following Operation and Maintenance Plan for the proposed project. This plan is broken into two major sections. The first section describes construction-related controls and practices. The second section is devoted to the post-construction operation and maintenance plan.

Basic Information

Developer:	Town of Sturbridge Senior Center
Contact:	Robyn Chrabascz, Facilities Manager
Address:	308 Main Street
City:	Sturbridge, MA 01566
Tel:	774-304-1408

Map of System Locations

See Drainage & Utilities Plan.

Good Housekeeping BMP's (Construction and Post Construction Periods)

The following good housekeeping practices will be followed onsite during and after the construction project:

- An effort will be made to store only enough product required to do the job. All materials stored onsite will be stored in a neat, orderly manner in their appropriate containers and, if possible under a roof or other enclosure
- Products will be kept in their original containers with the original manufacturer's label
- Substances will not be mixed with one another unless recommended by the manufacture
- Whenever possible, all of a product will be used up before disposing of the container
- Manufacturer's recommendations for proper use and disposal will be followed
- The site superintendent will inspect daily to ensure proper use and disposal of materials

CONSTRUCTION PERIOD

Material Handling And Waste Management

Hazardous Products:

These practices will be used to reduce the risks associated with hazardous materials. Material Safety Data Sheets (MSDSs) for each substance with hazardous properties that is used on the job site will be obtained and used for the proper management of potential wastes that may result from these products. An MSDS will be posted in the immediate area where such product is stored and/or used and another copy of each MSDS will be maintained in the SWPPP file at the job site construction trailer office. Each employee who must handle a substance with hazardous properties will be instructed on the use of MSDS sheets and the specific information in the applicable MSDS for the product they are using, particularly regarding spill control

techniques.

- Products will be kept in original containers unless they are not re-sealable
- Original labels and material safety data will be retained; they contain important product information
- If surplus product must be disposed of, manufacture's or local and State recommended methods for proper disposal will be followed

Hazardous Waste

All hazardous waste material will be disposed of by the Contractor in the manner specified by local, state, and/or federal regulations and by the manufacturer of such products. Site personnel will be instructed in these practices by the job site superintendent, who will also be responsible for seeing that these practices are followed.

Solid and Construction Wastes

All waste materials will be collected and stored in accordance with state and federal law in an appropriately covered container and/or securely lidded metal dumpster.

All trash and construction debris from the site will be deposited in the dumpster. No construction waste materials will be buried on site. All personnel will be instructed regarding the correct procedures for waste disposal.

All waste dumpsters and roll-off containers will be located in an area where the likelihood of the containers contributing to storm water discharges is negligible. If required, additional BMPs must be implemented, such as sandbags around the base, to prevent wastes from contributing to storm water discharges.

Sanitary Wastes

All sanitary waste will be collected from the portable units a minimum of three times per week by a licensed portable facility provider in complete compliance with local and state regulations.

All sanitary waste units will be located in an area where the likelihood of the unit contributing to storm water discharges is negligible. If required, additional BMP's must be implemented, such as sandbags around the base, to prevent wastes from contributing to storm water discharges.

Washout Areas

The Contractor will provide wheel wash stations and concrete washout areas at the site as described below.

Wheel Wash Stations

The Contractor will provide wheel wash stations adjacent to the construction entrance which lead directly to a public way or portions of the site outside the limits of work

Concrete Washout

Trucks will be allowed to washout or discharge surplus concrete or drum wash water on the site, but only in specifically designated diked and impervious washout areas which have been prepared to prevent contact between the concrete wash and stormwater. Waste generated from concrete wash water shall not be allowed to flow into drainage ways, inlets, receiving waters

or highway right of ways, or any location other than the designated concrete washout. Waste concrete may be poured into forms to make riprap or other useful concrete products. Proper signage designating the "concrete washout" shall be placed near the facility.

The hardened residue from the concrete washout diked areas will be disposed of in the same manner as other non-hazardous construction waste materials or may be broken up and used on site as deemed appropriate by the Contractor. Maintenance of the washout is to include removal of hardened concrete. Facility shall have sufficient volume to contain all the concrete waste resulting from washout and a minimum freeboard of 1 foot. Facility shall not be filled beyond 95% capacity and shall be cleaned out once 75% full unless a new facility is constructed.

Vehicle and Equipment Fueling

Areas will be designated on site, outside of any resource or buffer area, to refuel or maintain equipment used on site. Equipment fuel storage and refueling operations will be in an upland area at a horizontal distance greater than 100 feet from the boundaries of the wetland resource areas. The fueling areas will include secondary containment. The fueling areas will be inspected and cleaned weekly.

Spill Prevention and Control Plan

The Contractor will train all personnel in the proper handling and cleanup of spilled materials. No spilled hazardous materials or hazardous wastes will be allowed to come in contact with storm water discharges. If such contact occurs, the storm water discharge will be contained on site until appropriate measures in compliance with state and federal regulations are taken to dispose of such contaminated storm water. It shall be the responsibility of the job site superintendent to properly train all personnel in spill prevention and clean up procedures.

In order to minimize the potential for a spill of hazardous materials to come into contact with storm water, the following steps will be implemented:

- 1. All materials with hazardous properties (such as pesticides, petroleum products, fertilizers, detergents, construction chemicals, acids, paints, paint solvents, cleaning solvents, additives for soil stabilization, concrete curing compounds and additives, etc.) will be stored in a secure location, with their lids on, preferably under cover, when not in use.
- 2. During construction, liquid petroleum products and other hazardous materials with the potential to contaminate groundwater may not be stored or handled in areas of the site draining to an infiltration area, An "infiltration area" is any area of the site that by design or as a result of soils, topography and other relevant factors accumulates runoff that infiltrates into the soil. Dikes, berms, sumps, and other forms of secondary containment that prevent discharge to groundwater may be used to isolate portions of the site for the purposes of storage and handling of these materials
- 3. The minimum practical quantity of all such materials will be kept on the job site at all times.
- 4. A spill control and containment kit (containing, for example, absorbent materials, acid neutralizing powder, brooms, dust pans, mops, rags, gloves, goggles, plastic and metal trash containers, etc.) will be provided at the storage site. Catch basin inlet cover blankets and inflatable pipe plugs will be used to seal the openings in the outlet control structure and isolate product in the wet pond should a spill occur.
- 5. Manufacturer's recommended methods for spill cleanup will be clearly posted and site personnel will be trained

regarding these procedures and the location of the information and cleanup supplies.

In the event of a spill, the following procedures should be followed:

- 1. All spills will be cleaned up immediately after discovery.
- 2. The spill area will be kept well ventilated and personnel will wear appropriate protective clothing to prevent injury from contact with the hazardous substances.
- 3. The project manager and the Engineer of Record will be notified immediately.
- 4. Spills of toxic or hazardous materials will be reported to the appropriate federal, state, and/or local government agency, regardless of the size of the spill.
- 5. If the spill exceeds a Reportable Quantity, the SWPPP must be modified within seven (7) calendar days of knowledge of the discharge to provide a description of the release, the circumstances leading to the release, and the date of the release. The plans must identify measures to prevent the recurrence of such releases and to respond to such releases.

The job site superintendent will be the spill prevention and response coordinator. He will designate the individuals who will receive spill prevention and response training. These individuals will each become responsible for a particular phase of prevention and response. The names of these personnel will be posted in the material storage area and in the office trailer onsite.

Allowable Non-Stormwater Discharge Management

Certain types of discharges are allowed under the NPDES General Permit for Construction Activity, and it is the intent of this SWPPP to allow such discharges. These types of discharges will be allowed under the conditions that no pollutants will be allowed to come into contact with the water prior to or after its discharge. The control measures that have been outlined previously in this SWPPP will be strictly followed to ensure that no contamination of these non-stormwater discharges takes place. The following non-stormwater discharges that may occur from the job site include:

- Discharges from fire-fighting activities
- Waters used to wash vehicles where detergents are not used
- Water used to control dust in accordance with off-site vehicle tracking
- Pavement wash waters where spills or leaks of toxic or hazardous materials have not occurred (unless all spilled material has been removed) and where detergents are not used
- Uncontaminated ground water or spring water
- Uncontaminated excavation dewatering
- Landscape irrigation

POST CONSTRUCTION PERIOD

Post-Construction BMP's

The following best management practices are specified in the proposed development program to mitigate the increase in stormwater runoff from the site.

BMPs Used

- Deep Sump Catch Basins
- Proprietary Separators/Oil-Grease Separators
- Underground Infiltration System

Post-Development Activities

- 1. All sediments removed from the site drainage facilities shall be disposed of properly and in accordance with all applicable local and state regulations.
- 2. All vegetated slope areas on the site shall be stabilized following completion of construction and maintained to control erosion. Any disturbed areas shall be re-seeded and stabilized by the application of jute mesh if the slope exceeds 3 feet horizontal to 1 foot vertical.
- 3. Snow shall not be dumped into any waterbody, pond, wetland resource area, wet basin or detention basin.
- 4. The underground flood storage chambers and the inlet/outlet pipes shall be inspected a minimum of twice/year for signs of accumulated water or debris. Implement appropriate corrective action if any issues are discovered during the inspection. Cleaning shall be in strict conformance with the manufacturer's recommendations, which are attached to and made part of this Long Term Operation and Maintenance Plan.

All structural BMP's and maintenance responsibilities as identified on the site plans and within this document will be owned and maintained by the owner of the property and shall run with the title of the property.

Annual Reporting Form

The Owner shall keep complete records of all BMP maintenance activities using the following form:

OPERATION AND MAINTENANCE PLAN

Project: <u>480 Main Street</u> Location: <u>Sturbridge, M</u>

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Structure or Tack	Inspection	Inspection	Inspection Performed	Method	Notas/Bamarks
	Schedule	Date	By:	50130H	
Street Sweeping	April / May			Power broom or vacuum walks and pavement	
Deep Sump Catch Basin	March / June / September / November			Clam shell or vacuum sumps	Clean when sediment is 12'' deep
Proprietary Separator	March / June / September / November			Clam shell or vacuum sumps	Reduce to bi-annual inspections after first year of operations
Underground Infiltration System	April / May and October/ November			Inspect maintenance ports	Remove accumulated sediment.

Party responsible for O & M Plan:

Address <u>308 Main Street, Sturbridge, MA 01566</u> Contact <u>Robyn Chrabascz</u> Phone <u>774-304-1408</u> Name Sturbridge Senior Center

Annual Operating Budget

The estimated annual operating budget for the O & M Plan is \$2,000±.

Plan of BMP's

Reference is made to the proposed Drainage and Utilities plan for the location of all BMP's.

Post-Construction Snow Storage

Reference is made to the proposed Grading plan for the location of snow storage.

Maintenance of Natural Turf Areas

The Maintenance of Turf Areas (MTA) contains a program of maintenance practices to be used on this site. This program is designed to serve as the maintenance blueprint and describe materials used, rates of application and where possible, and expected time of application.

<u>Fertilizing</u>: No pesticides, fertilizers, and herbicides will be used within 100 foot buffer of wetlands. No salts quick release pesticides, quick release herbicides within 200 foot buffer of wetlands.

<u>Mowing:</u> Lawns will be mowed at a height of three (3) inches during the active growing season. Longer grass helps shade the soil and gather moisture, while competing more effectively with weeds. Mowing frequency will vary with the growing season and should be set by the plant height and not a set date. It will often be necessary to mow twice a week during periods of surge growth to help maintain plant health and color. Mowing should be less frequent during periods of heat and drought. The basic rule of thumb is to never remove more than 1/3 of the grass blade in one mowing. Removing more than half of the grass blade at a time can put the plant into shock, thus making it more susceptible to stress, disease and pests. A sharp mower blade is also key for clean cuts that heal quickly, versus a worn blade that invites disease and looks unsightly. A final mowing in November should be at two (2) inches to avoid matting and over wintering diseases.

<u>Clipping Management:</u> Clippings from all lawn areas will be left in place. Heavily clumped grass clippings are an indication of infrequent mowing, calling for an adjustment in the schedule. Heavy clumps must be raked in and dispersed by hand. Take care with the direction of mower machine movement - do not blow clippings into mulch beds and alternate patterns to assure an even cut and avoid soil compaction.

<u>Topdressing</u>: Topdressing is a practice of adding a small amount of sterile compost to the surface of the turf to reduce the development of thatch. Fine lawns will be topdressed annually with an approved source of composted organic matter, or as needed based on the turfgrass growth rate.

<u>Integrated Pest Management</u>: The basic goal and philosophy of the Integrated Pest Management (IPM) program is to produce a healthy, pest resistant lawn that will have little or no impact on the surrounding environment. Every available pest management practice will be utilized in order to not use pesticides. A new site provides the opportunity to construct a system that is less prone to stress, which is often the main cause of pest damage or invasion of weedy species.

The components of this IPM plan as established for New England sites are: proper grass selection, developing the site specific pest knowledge base, using action thresholds, soil, plant tissue and water testing, pest management options (cultural and biological) and yearly evaluation on the effectiveness of program and modification of plan.

It is anticipated that, after the first year of establishment of this site, weed problems will tend to be minimal. This is a result of sound site practices that will produce a dense, competitive environment against weed encroachment. Thus, the anticipated weeds on this site will be limited to broad leaf weeds and crabgrass, and less frequently moss. Weed control measures will be minimized to prevent runoff to the river area.

Standard 10: Prohibition of Illicit Discharges

As provided for in the 2008 MADEP Stormwater Handbook and the 2008 amendments to 310 CMR 10.00 et. seq. (MAWPA Regs) the following will serve as the Illicit Discharge Compliance Statement for the project.

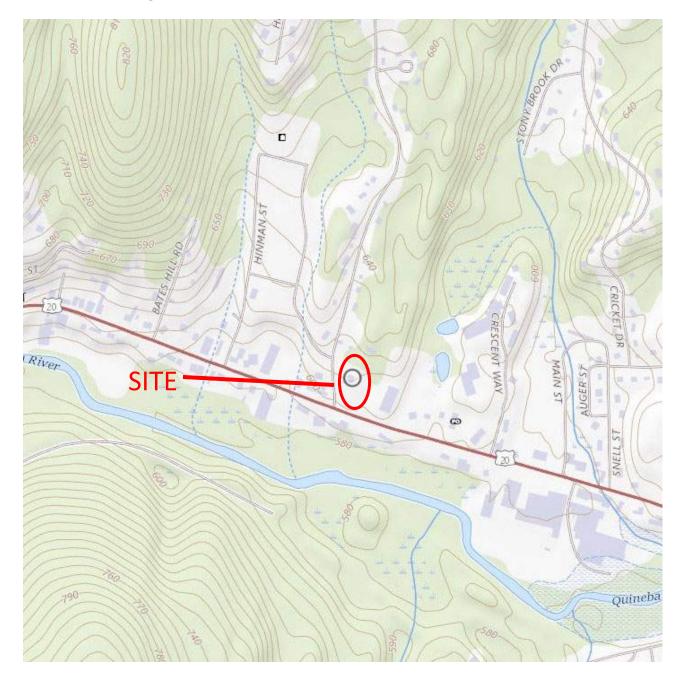
The existing developed site has no existing illicit discharges from the site. The new site is being designed such that there will not be any illicit discharges from the site.

Conclusion

As demonstrated in this report, the construction of the proposed development will meet the requirements of the the Stormwater Management Regulations of the Town of Sturbridge and the Site Plan Review criteria of the Town of Sturbridge Planning Board.

LOCUS MAP & NRCS SOIL MAP TEST PIT/SOILS DATA

Regional Locus 480 Main Street, Sturbridge, MA





United States Department of Agriculture

NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants Custom Soil Resource Report for Worcester County, Massachusetts, Southern Part



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report Soil Map



MAP	LEGEND	MAP INFORMATION
Area of Interest (AOI) Area of Interest (AOI) Soils	Spoil AreaStony Spot	The soil surveys that comprise your AOI were mapped at 1:25,000.
Soil Map Unit Polygons	 Very Stony Spot Wet Spot 	Warning: Soil Map may not be valid at this scale.
Soil Map Unit Lines	∆ Other	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil
Soil Map Unit Points Special Point Features	Special Line Features Water Features	line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed
BlowoutBorrow Pit	Streams and Canals	scale.
X Clay Spot	Transportation ++++ Rails	Please rely on the bar scale on each map sheet for map measurements.
Closed Depression	 Interstate Highways US Routes 	Source of Map: Natural Resources Conservation Service Web Soil Survey URL:
🚓 Gravelly Spot	Major Roads	Coordinate System: Web Mercator (EPSG:3857)
▲ Lava Flow▲ Marsh or swamp	Local Roads Background Aerial Photography	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.
Mine or Quarry Miscellaneous Water Perennial Water		This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.
Rock Outcrop Saline Spot		Soil Survey Area: Worcester County, Massachusetts, Southern Part Survey Area Data: Version 15, Sep 9, 2022
 Sandy Spot Severely Eroded Spot Sinkhole 		Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.
Slide or Slip Sodic Spot		Date(s) aerial images were photographed: Oct 15, 2020—Oct 31, 2020
		The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background

MAP LEGEND

MAP INFORMATION

imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
1	Water	0.9	2.5%
2A	Pootatuck fine sandy loam, 0 to 3 percent slopes, occasionally flooded	4.9	14.0%
3A	Scarboro and Walpole soils, 0 to 3 percent slopes	1.0	2.9%
71B	Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony	0.3	0.7%
305C	Paxton fine sandy loam, 8 to 15 percent slopes	2.7	7.8%
401B	Brookfield fine sandy loam, 3 to 8 percent slopes, extremely stony	8.2	23.5%
401C	Brookfield fine sandy loam, 8 to 15 percent slopes, extremely stony	1.5	4.2%
420B	Canton fine sandy loam, 3 to 8 percent slopes	14.1	40.3%
420C	Canton fine sandy loam, 8 to 15 percent slopes	1.4	4.1%
Totals for Area of Interest		35.0	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties

and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

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Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Worcester County, Massachusetts, Southern Part

1—Water

Map Unit Setting

National map unit symbol: 9bgp Mean annual precipitation: 32 to 50 inches Mean annual air temperature: 45 to 50 degrees F Frost-free period: 145 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Water: 100 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Water

Setting

Landform: Lakes

2A—Pootatuck fine sandy loam, 0 to 3 percent slopes, occasionally flooded

Map Unit Setting

National map unit symbol: 2zvdw Elevation: 150 to 770 feet Mean annual precipitation: 32 to 50 inches Mean annual air temperature: 45 to 50 degrees F Frost-free period: 145 to 240 days Farmland classification: All areas are prime farmland

Map Unit Composition

Pootatuck and similar soils: 75 percent Minor components: 25 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pootatuck

Setting

Landform: Flood plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear

Typical profile

O - 0 to 2 inches: muck
H2 - 2 to 12 inches: fine sandy loam
H3 - 12 to 27 inches: fine sandy loam
H4 - 27 to 65 inches: stratified gravelly coarse sand to loamy fine sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: About 19 to 23 inches
Frequency of flooding: Occasional
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: B Ecological site: F144AY012CT - Sandy Low Floodplain Hydric soil rating: No

Minor Components

Rippowam

Percent of map unit: 10 percent *Landform:* Alluvial flats *Hydric soil rating:* Yes

Occum

Percent of map unit: 10 percent Hydric soil rating: No

Whitman

Percent of map unit: 5 percent Landform: Depressions Hydric soil rating: Yes

3A—Scarboro and Walpole soils, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2svks Elevation: 160 to 480 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Scarboro and similar soils: 45 percent Walpole and similar soils: 35 percent Minor components: 20 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Scarboro

Setting

Landform: Drainageways, depressions, outwash deltas, outwash terraces Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Base slope, tread, dip

Down-slope shape: Concave

Across-slope shape: Concave

Parent material: Sandy glaciofluvial deposits derived from schist and/or sandy glaciofluvial deposits derived from gneiss and/or sandy glaciofluvial deposits derived from granite

Typical profile

Oe - 0 to 3 inches: mucky peat *A - 3 to 11 inches:* mucky fine sandy loam *Cg1 - 11 to 21 inches:* sand *Cg2 - 21 to 65 inches:* gravelly coarse sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (1.42 to 14.17 in/hr)
Depth to water table: About 0 to 2 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5w Hydrologic Soil Group: A/D Ecological site: F144AY031MA - Very Wet Outwash Hydric soil rating: Yes

Description of Walpole

Setting

Landform: Depressions on outwash plains, drainageways on outwash terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope, tread, dip, talf Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy and gravelly glaciofluvial deposits derived from granite and/or schist and/or gneiss

Typical profile

O - 0 to 2 inches: muck

A - 2 to 11 inches: fine sandy loam

Bg - 11 to 24 inches: fine sandy loam

Bw - 24 to 28 inches: sandy loam

Cg - 28 to 65 inches: sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: B/D Ecological site: F144AY028MA - Wet Outwash Hydric soil rating: Yes

Minor Components

Wareham

Percent of map unit: 10 percent Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Swansea

Percent of map unit: 10 percent Landform: Swamps, bogs Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

71B—Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony

Map Unit Setting

National map unit symbol: 2w69c Elevation: 0 to 1,290 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Ridgebury, extremely stony, and similar soils: 80 percent *Minor components:* 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ridgebury, Extremely Stony

Setting

Landform: Drumlins, depressions, ground moraines, hills, drainageways Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Head slope, base slope Down-slope shape: Concave Across-slope shape: Concave Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 6 inches: fine sandy loam

Bw - 6 to 10 inches: sandy loam

Bg - 10 to 19 inches: gravelly sandy loam

Cd - 19 to 66 inches: gravelly sandy loam

Properties and qualities

Slope: 3 to 8 percent
Surface area covered with cobbles, stones or boulders: 9.0 percent
Depth to restrictive feature: 15 to 35 inches to densic material
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: D Ecological site: F144AY009CT - Wet Till Depressions Hydric soil rating: Yes

Minor Components

Woodbridge, extremely stony

Percent of map unit: 10 percent Landform: Ground moraines, hills, drumlins Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Whitman, extremely stony

Percent of map unit: 8 percent Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Paxton, extremely stony

Percent of map unit: 2 percent Landform: Ground moraines, hills, drumlins Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Linear, convex Hydric soil rating: No

305C—Paxton fine sandy loam, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2w66y Elevation: 0 to 1,320 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Paxton and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Paxton

Setting

Landform: Ground moraines, hills, drumlins Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or schist

Typical profile

Ap - 0 to 8 inches: fine sandy loam Bw1 - 8 to 15 inches: fine sandy loam Bw2 - 15 to 26 inches: fine sandy loam Cd - 26 to 65 inches: gravelly fine sandy loam

Properties and qualities

Slope: 8 to 15 percent
Depth to restrictive feature: 20 to 39 inches to densic material
Drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: About 18 to 37 inches

Frequency of flooding: None *Frequency of ponding:* None *Maximum salinity:* Nonsaline (0.0 to 1.9 mmhos/cm) *Available water supply, 0 to 60 inches:* Low (about 4.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: C Ecological site: F144AY007CT - Well Drained Dense Till Uplands Hydric soil rating: No

Minor Components

Charlton

Percent of map unit: 7 percent Landform: Hills Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Woodbridge

Percent of map unit: 6 percent Landform: Hills, drumlins, ground moraines Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Side slope Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

Ridgebury

Percent of map unit: 2 percent Landform: Drumlins, drainageways, depressions, ground moraines, hills Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Head slope, base slope Down-slope shape: Concave, linear Across-slope shape: Concave, linear Hydric soil rating: Yes

401B—Brookfield fine sandy loam, 3 to 8 percent slopes, extremely stony

Map Unit Setting

National map unit symbol: 9bd2 Elevation: 510 to 1,020 feet Mean annual precipitation: 32 to 50 inches Mean annual air temperature: 45 to 50 degrees F Frost-free period: 145 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Brookfield and similar soils: 75 percent Minor components: 25 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Brookfield

Setting

Landform: Hills, ridges Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Convex Parent material: Friable coarse-loamy eolian deposits over friable coarse-loamy basal till derived from mica schist

Typical profile

O - 0 to 1 inches: muck H2 - 1 to 3 inches: fine sandy loam H3 - 3 to 32 inches: gravelly fine sandy loam H4 - 32 to 41 inches: gravelly loamy sand H5 - 41 to 65 inches: sandy loam

Properties and qualities

Slope: 3 to 8 percent
Surface area covered with cobbles, stones or boulders: 9.0 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: A Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Minor Components

Brimfield

Percent of map unit: 10 percent *Hydric soil rating:* No

Charlton

Percent of map unit: 10 percent Hydric soil rating: No

Paxton

Percent of map unit: 5 percent Hydric soil rating: No

401C—Brookfield fine sandy loam, 8 to 15 percent slopes, extremely stony

Map Unit Setting

National map unit symbol: 9bd3 Elevation: 560 to 970 feet Mean annual precipitation: 32 to 50 inches Mean annual air temperature: 45 to 50 degrees F Frost-free period: 145 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Brookfield and similar soils: 80 percent Minor components: 20 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Brookfield

Setting

Landform: Hills, ridges Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Linear Across-slope shape: Convex Parent material: Friable coarse-loamy eolian deposits over friable coarse-loamy basal till derived from mica schist

Typical profile

O - 0 to 1 inches: muck

H2 - 1 to 3 inches: fine sandy loam

H3 - 3 to 32 inches: gravelly fine sandy loam

- H4 32 to 41 inches: gravelly loamy sand
- H5 41 to 65 inches: sandy loam

Properties and qualities

Slope: 8 to 15 percent
Surface area covered with cobbles, stones or boulders: 9.0 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: A *Ecological site:* F144AY034CT - Well Drained Till Uplands *Hydric soil rating:* No

Minor Components

Brimfield

Percent of map unit: 10 percent Hydric soil rating: No

Charlton

Percent of map unit: 5 percent Hydric soil rating: No

Paxton

Percent of map unit: 5 percent Hydric soil rating: No

420B—Canton fine sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2w81b Elevation: 0 to 1,180 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: All areas are prime farmland

Map Unit Composition

Canton and similar soils: 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Canton

Setting

Landform: Hills, moraines, ridges Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

Typical profile

Ap - 0 to 7 inches: fine sandy loam Bw1 - 7 to 15 inches: fine sandy loam Bw2 - 15 to 26 inches: gravelly fine sandy loam 2C - 26 to 65 inches: gravelly loamy sand

Properties and qualities

Slope: 3 to 8 percent

Custom Soil Resource Report

Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural stratification
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Minor Components

Scituate

Percent of map unit: 10 percent Landform: Hills, drumlins, ground moraines Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Montauk

Percent of map unit: 5 percent Landform: Moraines, ground moraines, hills, drumlins Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Charlton

Percent of map unit: 4 percent Landform: Ridges, ground moraines, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Swansea

Percent of map unit: 1 percent Landform: Marshes, depressions, bogs, swamps, kettles Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

420C—Canton fine sandy loam, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2w817 Elevation: 0 to 1,330 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Canton and similar soils: 80 percent Minor components: 20 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Canton

Setting

Landform: Hills, moraines, ridges Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

Typical profile

Ap - 0 to 7 inches: fine sandy loam Bw1 - 7 to 15 inches: fine sandy loam Bw2 - 15 to 26 inches: gravelly fine sandy loam 2C - 26 to 65 inches: gravelly loamy sand

Properties and qualities

Slope: 8 to 15 percent
Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural stratification
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Minor Components

Montauk

Percent of map unit: 6 percent Landform: Moraines, ground moraines, hills, drumlins Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Scituate

Percent of map unit: 6 percent Landform: Hills, drumlins, ground moraines Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Side slope Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Newfields

Percent of map unit: 4 percent Landform: Ground moraines, hills, moraines Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Concave Hydric soil rating: No

Charlton

Percent of map unit: 4 percent Landform: Ridges, ground moraines, hills Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

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C. On-Site Review (continued)

Deep Observation Hole Number:

TP-1

Depth (in.)	Soil Horizon/	Soil Matrix: Color-	Redox	imorphic Fe (mottles)	eatures	Soil Texture		Fragments Volume	Soil	Soil Consistence	Other
Depth (m.)	Layer	Moist (Munsell)	Depth	Color	Percent	(USDA)	Gravel	Cobbles & Stones	Structure	(Moist)	Other
0-8"	Ар	2.5Y3/2				Fine Sandy Loam					
8-16"	В	10YR5/6				Sandy Loam					
16-35"	C1	2.5Y6/4				Sandy Loam	5%				
35-86"	C2	2.5Y6/3	36"			Sandy Loam	5%				

Additional Notes:

Mottles at 36". Weeping at 38" No Standing water.



TP-2

C. On-Site Review (continued)

Deep Observation Hole Number:

Depth (in.)	Soil Horizon/	Soil Matrix: Color- Moist (Munsell)		ximorphic Fe (mottles)	atures	Soil Texture	Coarse F % by V	ragments /olume	Soil	Soil Consistence	Other
Depth (m.)	Layer		Depth	Color	Percent	(USDA)	Gravel	Cobbles & Stone		(Moist)	
0-33"	Fill	10 YR 3/2				Fine Sandy Loam					
33"-36"	В	10YR4/6				Sandy Loam					
36"-65"	C1	2.5Y5/4				Sandy Loam					
65-75"	C2	2.5Y4/6	75"			Sand					
75-86"	C3	2.5Y5/4				Sandy Loam					

Additional Notes:

No Standing or weeping water.



C. On-Site Review (continued)

Deep Observation Hole Number:

TP-3

Depth (in.)	Soil Horizon/	Soil Matrix: Color-		imorphic Fe (mottles)	eatures	Soil Texture	Coarse % by	Fragments Volume	Soil	Soil Consistence	Other
Deptil (iii.)	Layer	Moist (Munsell)	Depth	Color	Percent	(USDA)	Gravel	Cobbles & Stones	Structure	(Moist)	
0-20"	Fill	10YR3/2				Fine Sandy Loam	5%	20%			
20-32"	В	10YR4/6				Sandy Loam	5%	10%			
32-82"	C1	2.5Y5/3	36"			Sandy Loam	5%	10%			

Additional Notes:

Mottles at 36". Weeping at 39". No Standing water.



TP-4

C. On-Site Review (continued)

Deep Observation Hole Number:

Depth (in.)	Soil Horizon/	Soil Matrix: Color-		kimorphic Fe (mottles)	atures	Soil Texture	% by `	Fragments Volume	Soil	Soil Consistence	Other
Depth (m.)	Layer	Moist (Munsell)	Depth	Color	Percent	(USDA)	Gravel	Cobbles & Stone		(Moist)	Other
0-55"	Fill	10 YR 3/2				Mix	20%	20%			
55"-85"	С	2.5Y5/3	65"			Sandy Loam					

Additional Notes:

Mottles at 65". No standing or weeping water.



C. On-Site Review (continued)

Deep Observation Hole Number:

TP-5

Depth (in.)	Soil Horizon/	Soil Matrix: Color-		imorphic Fe (mottles)	eatures	Soil Texture (USDA)	Coarse Fragments % by Volume		Soil	Soil Consistence	Other
Depth (m.)	Layer	Moist (Munsell)	Depth	Color	Percent		Gravel	Cobbles & Stones	Structure	(Moist)	Other
0-77"	FILL	10YR3/2									
77-96"	С	2.5Y3/2									

Additional Notes:

No Mottles. No Weeping. No Standing water.



TP-6

C. On-Site Review (continued)

Deep Observation Hole Number:

Depth (in.)	Soil Horizon/	Soil Matrix: Color-	Redoximorphic Features (mottles)		Soil Texture	% by \	ragments Volume	Soil	Soil Consistence	Other	
Deptil (III.)	Layer	Moist (Munsell)	Depth	Color	Percent	(USDA)	Gravel	Cobbles & Stone		(Moist)	
0-36"	FILL	10YR3/2				Fine Sandy Loam	20%	20%			
36-43"	Ab	10YR3/2				Fine Sandy Loam	5%				
43-66"	В	10YR5/6				Sandy Loam	5%				
66-96"	С	2.5Y3/2				Sandy Loam	5%				

Additional Notes:

No Mottles. No Weeping. No Standing water.

TSS REMOVAL CHARTS

2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings

3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row

4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row

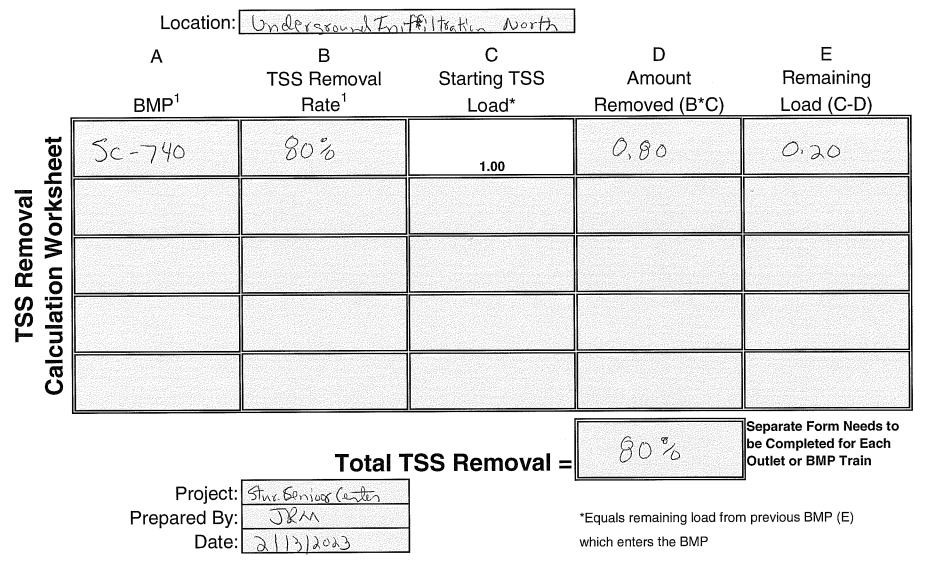
5. Total TSS Removal = Sum All Values in Column D $P_{xo} + t_{xo} + t_{xo}$

	Location:	Underssound Infil]						
	A BMP ¹	B TSS Removal Rate ¹	C Starting TSS Load*	D Amount Removed (B*C)	E Remaining Load (C-D)					
leet	Deep Sump Catch Basin	25%	1.00	Oids	0,75					
moval Worksheet	COSUNit	80%	0,75	0,60	0,15					
(1)										
TSS Re Calculation										
Calo										
		Total T	SS Removal =	85%	Separate Form Needs to be Completed for Each Outlet or BMP Train					
Project: <u>Stw. Semion (2, 19)</u> Prepared By: <u>JRM</u> *Equals remaining load from previous BMP (E) Date: <u>2(13)</u> 2023 which enters the BMP										

Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1

2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings

- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row
- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D



Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1

2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings

3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row

4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row

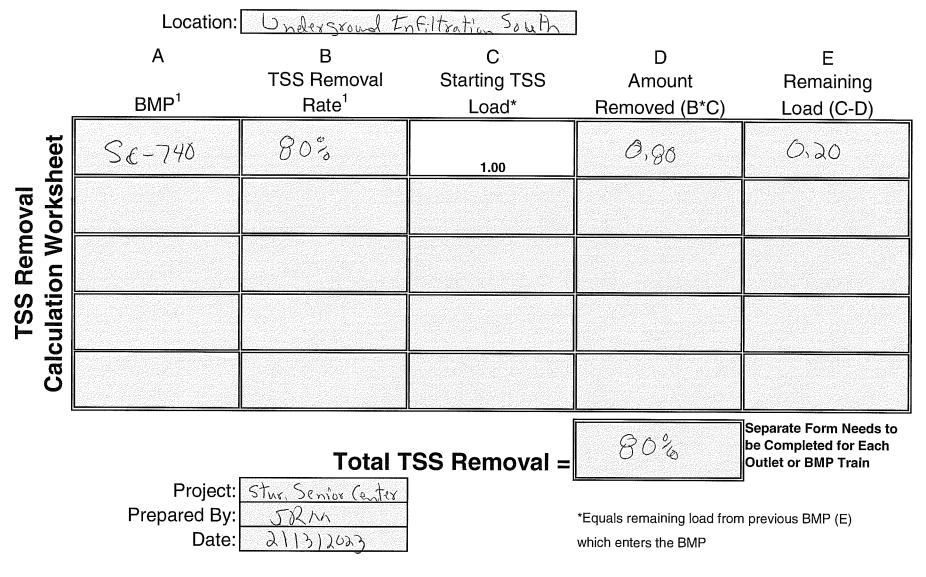
5. Total TSS Removal = Sum All Values in Column D $\int_{\mathcal{F}} t_{\mathcal{F}} t_{\mathcal{$

	Location:	Under social Inf]						
	A	В	C	D	E					
_	BMP ¹	TSS Removal Rate ¹	Starting TSS Load*	Amount Removed (B*C)	Remaining Load (C-D)					
leet	D-eep Surp Catch Masin	२ <i>९%</i>	1.00	0125	0.75					
moval Worksheet	COSUNIT	80%	0,75	0,60	0,15					
TSS Re Calculation										
Calc										
Total TSS Removal = 영웅왕 Outlet or BMP Train										
	Project: Stus, Senios Cater Prepared By: JRM Date: 2//3/2023 which enters the BMP									

1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table

2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings

- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row
- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D



Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1





CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION **BASED ON THE RATIONAL RAINFALL METHOD** STURBRIDGE SENIOR CENTER STURBRIDGE, MA 0.76 ac Unit Site Designation **PS#1** Area Rainfall Station # Weighted C 0.9 70 6 min t_c CDS Model 2015-4 **CDS** Treatment Capacity 1.4 cfs Rainfall Percent Rainfall Cumulative Total Flowrate **Treated Flowrate** Incremental Intensity¹ Volume¹ **Rainfall Volume** Removal (%) (cfs) (cfs) (in/hr) 0.04 15.1% 15.1% 0.03 0.03 14.5 0.05 0.05 23.2 0.08 24.6% 39.7% 0.12 13.7% 53.4% 0.08 0.08 12.8 0.16 9.4% 62.8% 0.11 0.11 8.7 0.20 6.6% 69.5% 0.14 0.14 6.0 0.24 5.2% 74.7% 0.16 0.16 4.7 0.28 4.8% 79.5% 0.19 0.19 4.2 0.32 3.1% 82.6% 0.22 0.22 2.7 0.36 2.7% 85.3% 0.24 0.24 2.3 0.40 2.1% 87.4% 0.27 0.27 1.8 0.48 2.5% 89.9% 0.33 0.33 2.0 2.0% 0.56 91.9% 0.38 0.38 1.6 0.64 1.4% 93.3% 0.43 0.43 1.1 0.72 1.0% 94.3% 0.49 0.49 0.7 0.54 0.80 1.1% 95.4% 0.54 0.8 1.00 1.6% 97.1% 0.68 0.68 1.1 0.9% 1.20 98.0% 0.82 0.82 0.5 0.3 1.40 0.6% 0.95 0.95 98.6% 1.60 0.5% 99.1% 1.09 1.09 0.2 1.22 1.22 0.2 1.80 0.5% 99.6% 0.00 0.0% 99.6% 0.00 0.00 0.0 89.3 Removal Efficiency Adjustment² = 0.0% Predicted % Annual Rainfall Treated = 99.6% Predicted Net Annual Load Removal Efficiency = 89.3% 1 - Based on 14 years of 15-minute rainfall data from NCDC Station 2107, East Brimfield Lake, Worcester County, N 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.





CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION **BASED ON THE RATIONAL RAINFALL METHOD** STURBRIDGE SENIOR CENTER STURBRIDGE , MA 0.44 ac Unit Site Designation **PS#2** Area 0.9 Rainfall Station # Weighted C 70 6 min t_c CDS Model 1515-3 **CDS** Treatment Capacity 1.0 cfs Rainfall Percent Rainfall Cumulative Total Flowrate **Treated Flowrate** Incremental Intensity¹ Volume¹ **Rainfall Volume** Removal (%) (cfs) (cfs) (in/hr) 0.04 15.1% 15.1% 0.02 0.02 14.6 0.03 0.08 24.6% 39.7% 0.03 23.4 0.12 13.7% 53.4% 0.05 0.05 12.9 0.16 9.4% 62.8% 0.06 0.06 8.7 0.20 6.6% 69.5% 0.08 0.08 6.1 0.24 5.2% 74.7% 0.09 0.09 4.8 4.8% 0.28 79.5% 0.11 0.11 4.3 0.32 3.1% 82.6% 0.13 0.13 2.8 0.36 2.7% 85.3% 0.14 0.14 2.4 0.40 2.1% 87.4% 0.16 0.16 1.8 0.48 2.5% 89.9% 0.19 0.19 2.1 2.0% 0.22 1.7 0.56 91.9% 0.22 0.64 1.4% 93.3% 0.25 0.25 1.1 0.72 1.0% 94.3% 0.28 0.28 0.8 0.80 1.1% 95.4% 0.31 0.31 0.8 1.00 1.6% 97.1% 0.39 0.39 1.2 0.9% 1.20 98.0% 0.47 0.47 0.6 1.40 0.6% 0.55 0.55 0.4 98.6% 1.60 0.5% 99.1% 0.63 0.63 0.3 0.71 0.2 1.80 0.5% 99.6% 0.71 0.00 0.0% 99.6% 0.00 0.00 0.0 90.8 Removal Efficiency Adjustment² = 0.0% Predicted % Annual Rainfall Treated = 99.6% Predicted Net Annual Load Removal Efficiency = 90.8% 1 - Based on 14 years of 15-minute rainfall data from NCDC Station 2107, East Brimfield Lake, Worcester County, N 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

Project: Location: Prepared For:	Sturbridge Senior Center Sturbridge , MA Waterfield Design Group	C NTECH ENGINEERED SOLUTIONS					
<u>Purpose:</u>	To calculate the water quality flow rate (WQF) over a given site area. In this situation the WQF is derived from the first 1" of runoff from the contributing impervious surface.						
Reference:	Massachusetts Dept. of Environmental Protection Wetlands Program / United States Department of Agriculture Natural Resources Conservation Service TR-55 Manual						
Procedure:	Determine unit peak discharge using Figure 1 or 2. Figure 2 is in tabular for the tc, read the unit peak discharge (qu) from Figure 1 or Table in Figure 2 following units: cfs/mi ² /watershed inches (csm/in).						
	Compute Q Rate using the following equation:						
	Q = (qu) (A) (WQV)						
	where: Q = flow rate associated with first 1" of runoff						

qu = the unit peak discharge, in csm/in.
A = impervious surface drainage area (in square miles)
WQV = water quality volume in watershed inches (1" in this case)

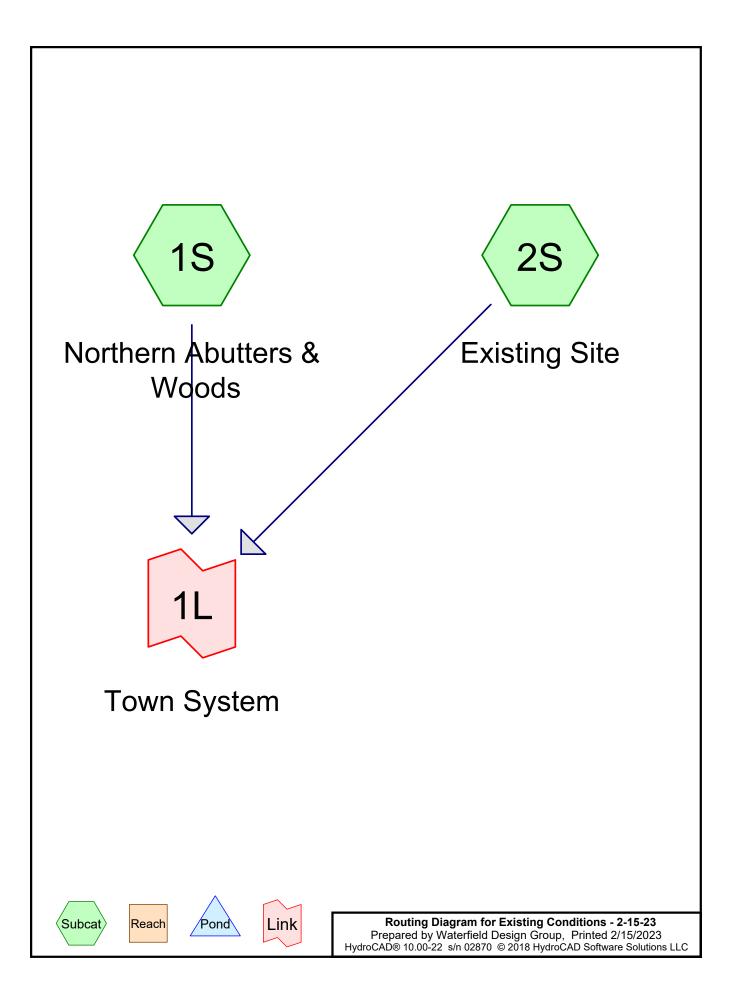
Structure Name	Impv. (acres)	A (miles ²)	t _c (min)	t _c (hr)	WQV (in)	qu (csm/in.)	Q (cfs)
PS#1	0.76	0.0011797	6.0	0.100	1.00	774.00	0.91
PS#2	0.44	0.0006813	6.0	0.100	1.00	774.00	0.53

RECHARGE CALCULATIONS & 1" VOLUME INFILTRATION

Project Name:	Town of Sturbridge Senior Ce	enter	Sheet No.:	1			
Done by:	JRM		Date:	2/17/2023			
Recharge Volume Calculations							
480 Main Street							
Paved Area (HSG B) =	40,075.2 SF						
Infiltration Volume							
HSG B Volume =	.35"/12 0.0	.029167 ft.					
Volume .029167 ft. * 40,075 SF	1,169 cu. ft.						
Underground Infiltration System Vo	lume Provided (From HCAD) =	15,94	10 cu. ft.				
Retain 1" of Total Post-Construction	Impervious Surface						
1" Volume =	1"/12 0.	.083333 ft.					
Volume = .083333 ft. * 40,075 SF	3,340 cu. ft.						
Underground Infiltration System Vo	lume Provided (From HCAD) =	15,94	10 cu. ft.				
Underground Infiltration System Re	ar						
Bottom of Stone Elevation = High Groundwater Elevation = 3.2' > 2.0' Required	607.5 604.3						
Time to empty based on Rawls Rate	for B Soils:						
610.75 - 607.50 = 3.25' = 39"							
Time to empty = 39"/1.02 in./hr. = 3	8.3 hrs.						
38.3 hrs. < 72 hrs.							
Underground Infiltration System Fro	ont						
Bottom of Stone Elevation = High Groundwater Elevation = 3.0' > 2.0' Required	600.5 597.5						
Time to empty based on Rawls Rate for B Soils:							
603.75 - 600.50 = 3.25' = 39"	603.75 - 600.50 = 3.25' = 39"						
Time to empty = 39"/1.02 in./hr. = 3	8.3 hrs.						
38.3 hrs. < 72 hrs.							

EXISTING CONDITIONS

RUNOFF & VOLUME CALCULATIONS (2, 10, & 100 YEAR STORMS)



Existing Conditions - 2-15-23	Type III 24-hr	2 YR Rain	nfall=3.13"
Prepared by Waterfield Design Group		Printed	2/15/2023
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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Northern Abutters &	Runoff Area=129,244 sf 12.22% Impervious Runoff Depth=0.65" Flow Length=927' Tc=42.7 min CN=67 Runoff=0.89 cfs 0.161 af
Subcatchment 2S: Existing Site	Runoff Area=53,232 sf 37.77% Impervious Runoff Depth=1.35" Flow Length=250' Tc=6.0 min CN=80 Runoff=1.87 cfs 0.137 af
Link 1L: Town System	Inflow=1.94 cfs 0.298 af

Primary=1.94 cfs 0.298 af

Page 2

Summary for Subcatchment 1S: Northern Abutters & Woods

Runoff = 0.89 cfs @ 12.69 hrs, Volume= 0.161 af, Depth= 0.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YR Rainfall=3.13"

_	A	rea (sf)	CN	Description						
*		6,719	98	Paved Road HSB B						
		30,242		50-75% Grass cover, Fair, HSG B						
*		9,074		Buildings	•	, -				
		83,209		Woods, Fai	r, HSG B					
		129,244		Weighted A						
		113,451		87.78% Per	•					
		15,793		12.22% Imp						
		10,100		1 —11— 275r						
	Тс	Length	Slope	e Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)		(cfs)					
	28.3	100	0.0100	//	· · · ·	Sheet Flow, Sheet Flow				
			••••			Woods: Light underbrush $n= 0.400 P2= 3.20"$				
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow				
	-					Short Grass Pasture Kv= 7.0 fps				
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Wood	ls			
	-		•			Woodland Kv= 5.0 fps				
	2.3	200	0.0500) 1.42	31.29		1			
						Area= 22.0 sf Perim= 12.0' r= 1.83' n= 0.350				
	0.3	200	0.0150) 13.10	786.18	Channel Flow, Draing Channel #2				
						Area= 60.0 sf Perim= 15.0' r= 4.00' n= 0.035				
	42.7	927	Total							

Purpose the second seco

Subcatchment 1S: Northern Abutters & Woods

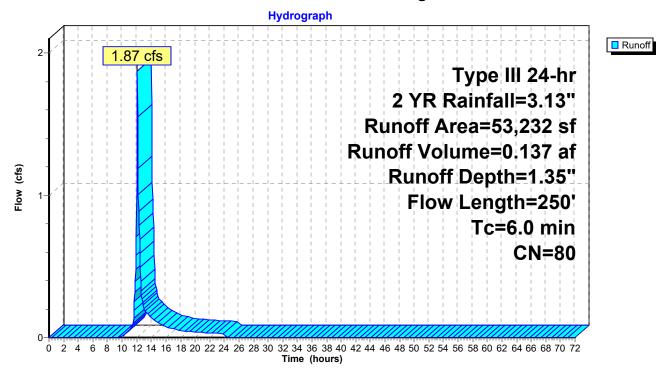
Summary for Subcatchment 2S: Existing Site

Runoff = 1.87 cfs @ 12.10 hrs, Volume= 0.137 af, Depth= 1.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YR Rainfall=3.13"

_	A	rea (sf)	CN E	escription						
*		16,831	98 F	Paved Road HSB B						
		33,128	69 5	0-75% Grass cover, Fair, HSG B						
*		3,273	98 E	Buildings						
		53,232	80 V	Veighted A	verage					
		33,128	6	2.23% Per	vious Area					
		20,104	3	7.77% Imp	pervious Are	ea				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	1.2	100	0.0200	1.38		Sheet Flow, Pavement				
						Smooth surfaces n= 0.011 P2= 3.20"				
	1.6	150	0.0500	1.57		Shallow Concentrated Flow, Lawn				
						Short Grass Pasture Kv= 7.0 fps				
_	3.2					Direct Entry, Direct Entry				
	6.0	250	Total							

Subcatchment 2S: Existing Site

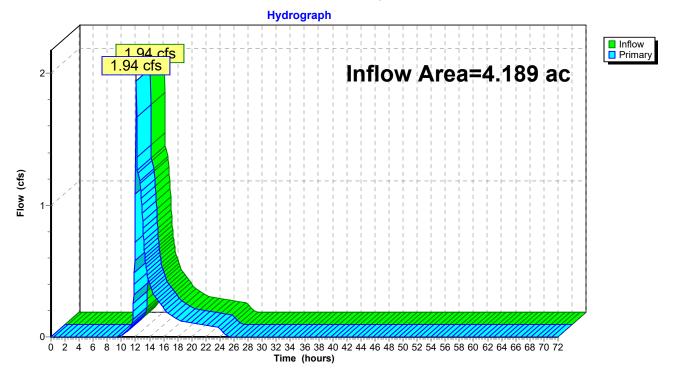


Summary for Link 1L: Town System

Inflow Area	=	4.189 ac, 19.67% Impervious, Inflow Depth = 0.85" for 2 YR event
Inflow	=	1.94 cfs @ 12.10 hrs, Volume= 0.298 af
Primary	=	1.94 cfs $@$ 12.10 hrs, Volume= 0.298 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 1L: Town System



Existing Conditions - 2-15-23	Type III 24-hr	10 YR Rair	nfall=4.64"
Prepared by Waterfield Design Group		Printed	2/15/2023
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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Northern Abutters &	Runoff Area=129,244 sf 12.22% Impervious Runoff Depth=1.56" Flow Length=927' Tc=42.7 min CN=67 Runoff=2.45 cfs 0.385 af
Subcatchment 2S: Existing Site	Runoff Area=53,232 sf 37.77% Impervious Runoff Depth=2.58" Flow Length=250' Tc=6.0 min CN=80 Runoff=3.63 cfs 0.263 af
Link 1L: Town System	Inflow=4.12 cfs 0.648 af

Primary=4.12 cfs 0.648 af

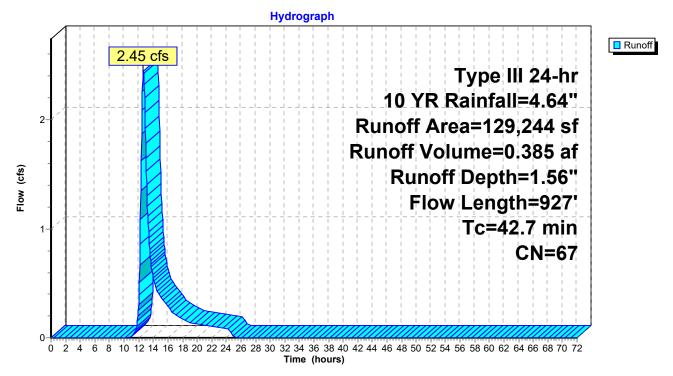
Summary for Subcatchment 1S: Northern Abutters & Woods

Runoff = 2.45 cfs @ 12.63 hrs, Volume= 0.385 af, Depth= 1.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YR Rainfall=4.64"

_	Α	vrea (sf)	CN	Description							
*		6,719	98	Paved Road HSB B							
		30,242	69	50-75% Gr	50-75% Grass cover, Fair, HSG B						
*		9,074		Buildings							
		83,209		Woods, Fai	ır, HSG B						
	1	129,244		Weighted A	•						
		113,451		87.78% Per							
		15,793			pervious Are						
		-)		•							
	Тс	Length	Slope	e Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)		(cfs)	·					
_	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow	ļ				
						Woods: Light underbrush n= 0.400 P2= 3.20"					
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow					
						Short Grass Pasture Kv= 7.0 fps					
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woo	ods				
						Woodland Kv= 5.0 fps	l				
	2.3	200	0.0500) 1.42	31.29	Channel Flow, Drain Channel #1	l				
						Area= 22.0 sf Perim= 12.0' r= 1.83' n= 0.350					
	0.3	200	0.0150) 13.10	786.18	Channel Flow, Draing Channel #2]				
_						Area= 60.0 sf Perim= 15.0' r= 4.00' n= 0.035					
	42.7	927	Total								

Subcatchment 1S: Northern Abutters & Woods



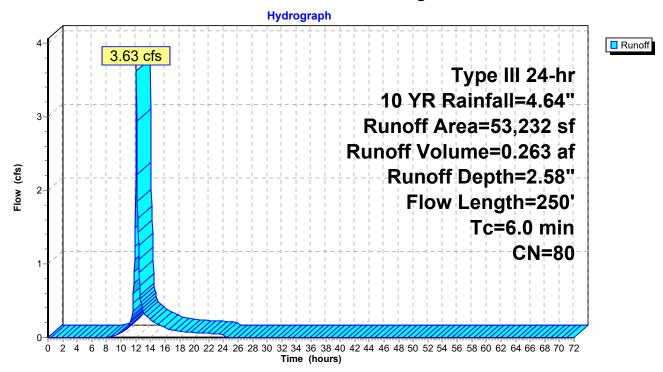
Summary for Subcatchment 2S: Existing Site

Runoff = 3.63 cfs @ 12.09 hrs, Volume= 0.263 af, Depth= 2.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YR Rainfall=4.64"

_	A	rea (sf)	CN D	escription					
*		16,831	98 F	Paved Road HSB B					
		33,128	69 5	0-75% Grass cover, Fair, HSG B					
*		3,273	98 E	luildings					
		53,232	80 V	Veighted A	verage				
		33,128	6	2.23% Per	vious Area				
		20,104	3	7.77% Imp	pervious Are	ea			
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	1.2	100	0.0200	1.38		Sheet Flow, Pavement			
						Smooth surfaces n= 0.011 P2= 3.20"			
	1.6	150	0.0500	1.57		Shallow Concentrated Flow, Lawn			
						Short Grass Pasture Kv= 7.0 fps			
_	3.2					Direct Entry, Direct Entry			
	6.0	250	Total						

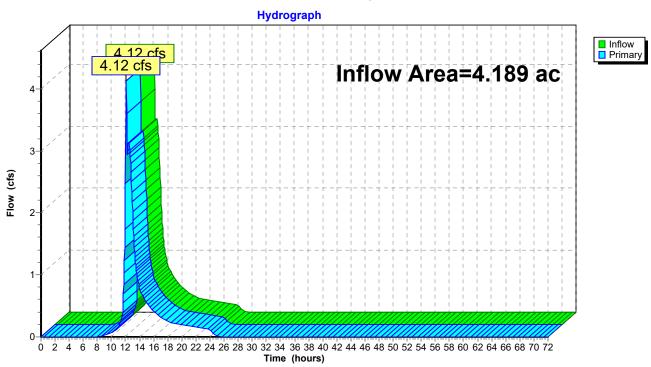
Subcatchment 2S: Existing Site



Summary for Link 1L: Town System

Inflow Area	a =	4.189 ac, 19.67% Impervious, Inflow Depth = 1.86" for 10 YR even	t
Inflow	=	4.12 cfs @ 12.10 hrs, Volume= 0.648 af	
Primary	=	4.12 cfs $ ilde{@}$ 12.10 hrs, Volume= 0.648 af, Atten= 0%, Lag= 0.0) min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Link 1L: Town System

Existing Conditions - 2-15-23	Type III 24-hr	25 YR Rair	nfall=5.81"
Prepared by Waterfield Design Group		Printed	2/15/2023
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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Northern Abutters &	Runoff Area=129,244 sf 12.22% Impervious Runoff Depth=2.39" Flow Length=927' Tc=42.7 min CN=67 Runoff=3.87 cfs 0.590 af
Subcatchment 2S: Existing Site	Runoff Area=53,232 sf 37.77% Impervious Runoff Depth=3.61" Flow Length=250' Tc=6.0 min CN=80 Runoff=5.05 cfs 0.368 af
Link 1L: Town System	Inflow=6.00 cfs 0.958 af

Primary=6.00 cfs 0.958 af

Summary for Subcatchment 1S: Northern Abutters & Woods

Runoff = 3.87 cfs @ 12.61 hrs, Volume= 0.590 af, Depth= 2.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YR Rainfall=5.81"

_	Α	rea (sf)	CN I	Description	1					
*		6,719	98	Paved Roa	Paved Road HSB B					
		30,242		50-75% Gr/	ass cover, F	Fair, HSG B	l			
*		9,074		Buildings		, -	l			
		83,209		Woods, Fai	ır, HSG B		ļ			
		29,244		Weighted A			l			
		13,451		87.78% Per			l			
		15,793			pervious Are		ļ			
		,		•			ļ			
	Тс	Length	Slope	e Velocity	Capacity	Description	ļ			
_	(min)	(feet)	(ft/ft)		(cfs)		l			
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow				
						Woods: Light underbrush n= 0.400 P2= 3.20"				
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow	l			
						Short Grass Pasture Kv= 7.0 fps				
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woo	ods			
						Woodland Kv= 5.0 fps				
	2.3	200	0.0500) 1.42	31.29	Channel Flow, Drain Channel #1				
						Area= 22.0 sf Perim= 12.0' r= 1.83' n= 0.350				
	0.3	200	0.0150) 13.10	786.18					
_						Area= 60.0 sf Perim= 15.0' r= 4.00' n= 0.035				
	42.7	927	Total							

Hydrograph Runoff 3.87 cfs 4 Type III 24-hr 25 YR Rainfall=5.81" Runoff Area=129,244 sf 3-Runoff Volume=0.590 af Flow (cfs) Runoff Depth=2.39" Flow Length=927' 2 Tc=42.7 min CN=67 1 0 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

Subcatchment 1S: Northern Abutters & Woods

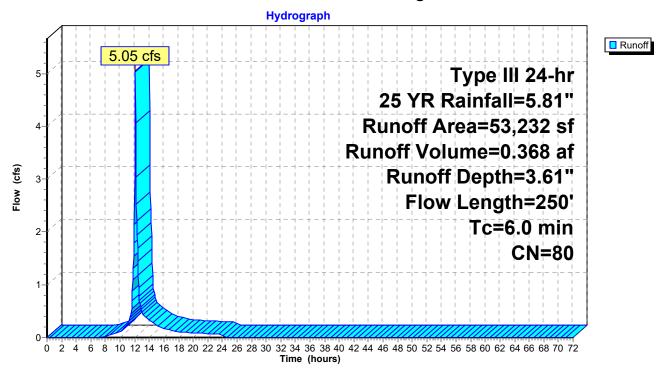
Summary for Subcatchment 2S: Existing Site

Runoff = 5.05 cfs @ 12.09 hrs, Volume= 0.368 af, Depth= 3.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YR Rainfall=5.81"

_	A	rea (sf)	CN E	escription		
*		16,831	98 F	aved Road	d HSB B	
		33,128	69 5	0-75% Gra	ass cover, F	Fair, HSG B
*		3,273	98 E	luildings		
		53,232	80 V	Veighted A	verage	
		33,128	6	2.23% Per	vious Area	
		20,104	3	7.77% Imp	pervious Are	ea
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.2	100	0.0200	1.38		Sheet Flow, Pavement
						Smooth surfaces n= 0.011 P2= 3.20"
	1.6	150	0.0500	1.57		Shallow Concentrated Flow, Lawn
						Short Grass Pasture Kv= 7.0 fps
	3.2					Direct Entry, Direct Entry
	6.0	250	Total			

Subcatchment 2S: Existing Site

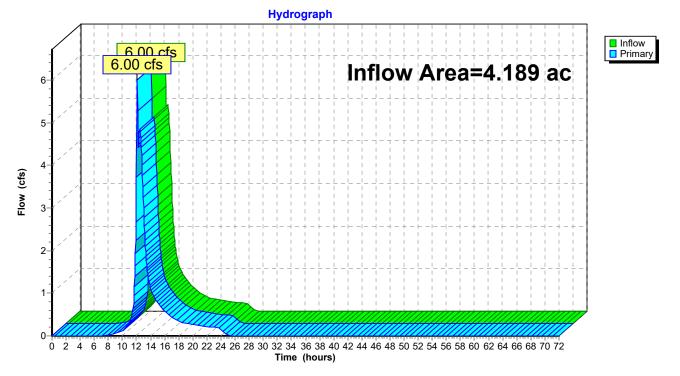


Summary for Link 1L: Town System

Inflow Area	=	4.189 ac, 19.67% Impervious, Inflow Depth = 2.74" for 25 YR event	
Inflow	=	6.00 cfs @ 12.10 hrs, Volume= 0.958 af	
Primary	=	6.00 cfs $ ilde{@}$ 12.10 hrs, Volume= 0.958 af, Atten= 0%, Lag= 0.0 mi	n

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 1L: Town System



Existing Conditions - 2-15-23	Type III 24-hr	100 YR Rain	nfall=8.19"
Prepared by Waterfield Design Group		Printed	2/15/2023
HydroCAD® 10.00-22 s/n 02870 © 2018 HydroCAD Software Solution	ns LLC		Page 17

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Northern Abutters &	Runoff Area=129,244 sf 12.22% Impervious Runoff Depth=4.28" Flow Length=927' Tc=42.7 min CN=67 Runoff=7.07 cfs 1.058 af
Subcatchment 2S: Existing Site	Runoff Area=53,232 sf 37.77% Impervious Runoff Depth=5.80" Flow Length=250' Tc=6.0 min CN=80 Runoff=7.99 cfs 0.591 af
Link 1L: Town System	Inflow=10.04 cfs 1.649 af

Inflow=10.04 cfs 1.649 af Primary=10.04 cfs 1.649 af

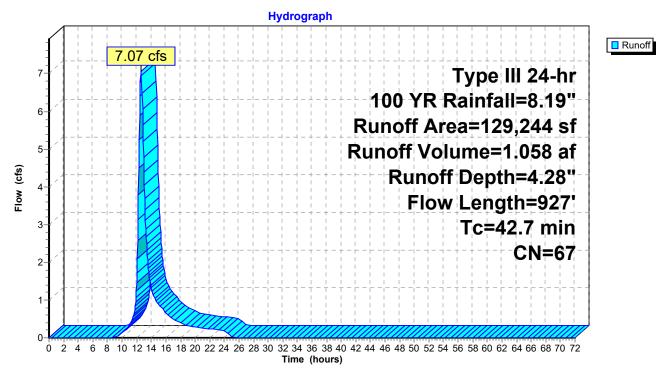
Summary for Subcatchment 1S: Northern Abutters & Woods

Runoff = 7.07 cfs @ 12.60 hrs, Volume= 1.058 af, Depth= 4.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YR Rainfall=8.19"

_	Α	rea (sf)	CN	Description	1					
*		6,719	98	Paved Roa	Paved Road HSB B					
		30,242		50-75% Gr	ass cover, F	Fair, HSG B				
*		9,074		Buildings	-	,				
		83,209		Woods, Fai	ır, HSG B					
_		129,244		Weighted A	,					
		113,451		87.78% Per	•	1				
		15,793			pervious Are					
		,								
	Тс	Length	Slope	e Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)		(cfs)	•				
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow				
						Woods: Light underbrush n= 0.400 P2= 3.20"				
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow				
						Short Grass Pasture Kv= 7.0 fps				
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Wood	ds			
						Woodland Kv= 5.0 fps				
	2.3	200	0.0500) 1.42	31.29	Channel Flow, Drain Channel #1				
						Area= 22.0 sf Perim= 12.0' r= 1.83' n= 0.350				
	0.3	200	0.0150) 13.10	786.18					
_						Area= 60.0 sf Perim= 15.0' r= 4.00' n= 0.035				
	42.7	927	Total							

Subcatchment 1S: Northern Abutters & Woods



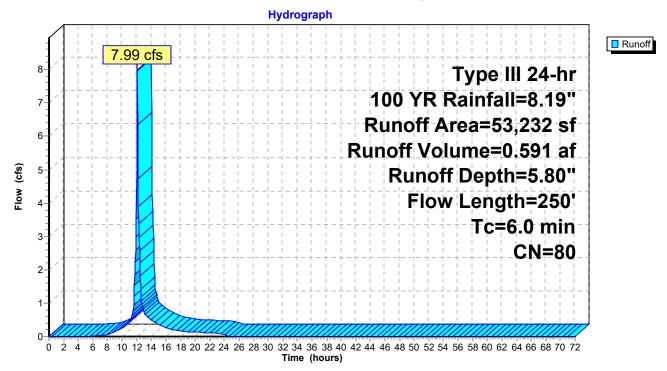
Summary for Subcatchment 2S: Existing Site

Runoff = 7.99 cfs @ 12.09 hrs, Volume= 0.591 af, Depth= 5.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YR Rainfall=8.19"

	A	rea (sf)	CN E	escription		
*		16,831	98 F	aved Road	d HSB B	
		33,128	69 5	0-75% Gra	ass cover, F	Fair, HSG B
*		3,273	98 E	luildings		
		53,232	80 V	Veighted A	verage	
		33,128	6	2.23% Per	vious Area	
		20,104	3	7.77% Imp	pervious Ar	ea
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.2	100	0.0200	1.38		Sheet Flow, Pavement
						Smooth surfaces n= 0.011 P2= 3.20"
	1.6	150	0.0500	1.57		Shallow Concentrated Flow, Lawn
						Short Grass Pasture Kv= 7.0 fps
	3.2					Direct Entry, Direct Entry
	6.0	250	Total			

Subcatchment 2S: Existing Site

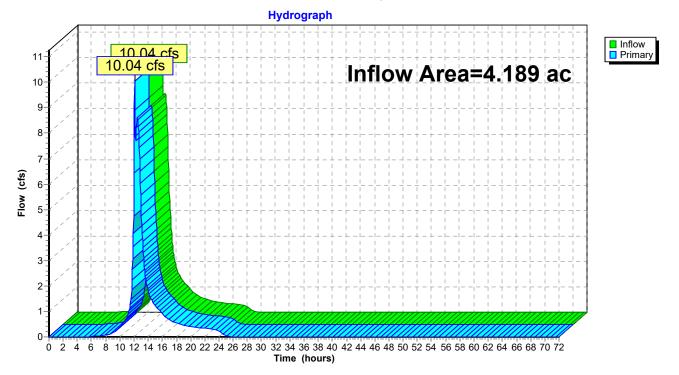


Summary for Link 1L: Town System

Inflow Area	a =	4.189 ac, 19.67% Impervious, Inflow Depth = 4.72" for 100 YR event	
Inflow	=	0.04 cfs @ 12.10 hrs, Volume= 1.649 af	
Primary	=	0.04 cfs @ 12.10 hrs, Volume= 1.649 af, Atten= 0%, Lag= 0.0 min	

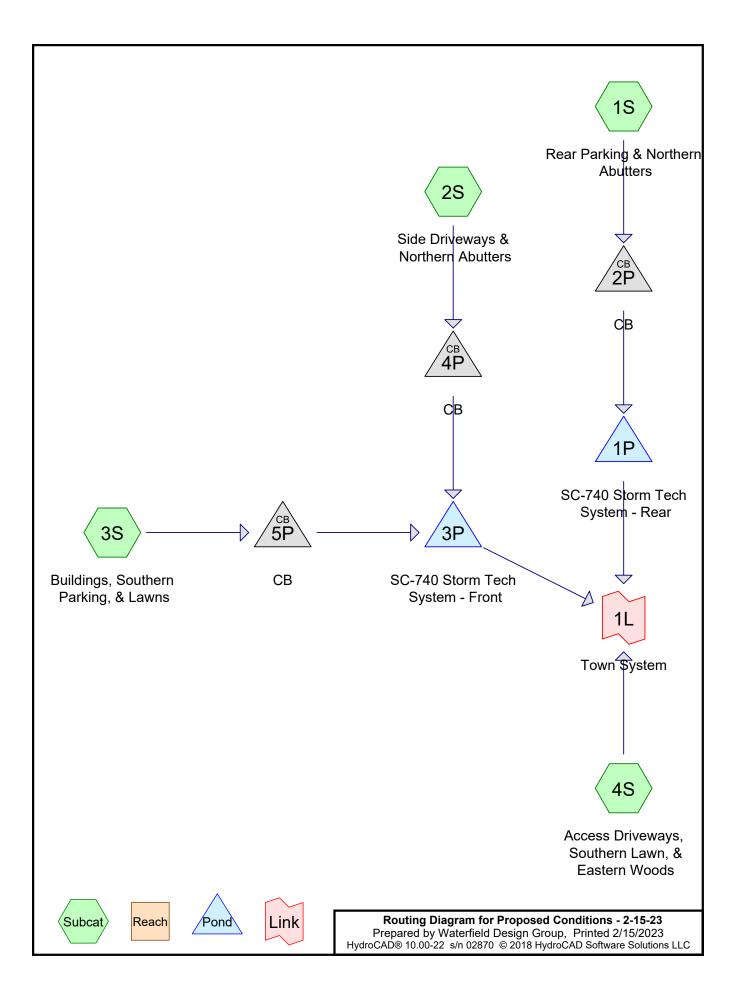
Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 1L: Town System



PROPOSED (SITE DEVELOPED) CONDITIONS

RUNOFF & VOLUME CALCULATIONS (2, 10, & 100 YEAR STORMS)



Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Rear Parking &	Runoff Area=72,157 sf 26.36% Impervious Runoff Depth=0.01" Flow Length=527' Tc=40.1 min CN=72 Runoff=0.00 cfs 0.002 af
Subcatchment2S: Side Driveways &	Runoff Area=34,445 sf 36.79% Impervious Runoff Depth=0.05" Flow Length=527' Tc=40.1 min CN=77 Runoff=0.01 cfs 0.003 af
Subcatchment3S: Buildings, Southern	Runoff Area=35,108 sf 57.63% Impervious Runoff Depth=0.36" Tc=6.0 min CN=91 Runoff=0.32 cfs 0.024 af
Subcatchment4S: Access Driveways,	Runoff Area=40,758 sf 7.04% Impervious Runoff Depth=0.00" Flow Length=579' Tc=33.3 min CN=68 Runoff=0.00 cfs 0.000 af
Pond 1P: SC-740 Storm Tech System - F Discarded=0.00	Rear Peak Elev=607.50' Storage=1 cf Inflow=0.00 cfs 0.002 af 0 cfs 0.002 af Primary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.002 af
Pond 2P: CB 12.0" Rou	Peak Elev=609.32' Inflow=0.00 cfs 0.002 af Ind Culvert n=0.013 L=95.0' S=0.0100 '/' Outflow=0.00 cfs 0.002 af
Pond 3P: SC-740 Storm Tech System - F Discarded=0.1	Front Peak Elev=600.56' Storage=156 cf Inflow=0.32 cfs 0.027 af 5 cfs 0.027 af Primary=0.00 cfs 0.000 af Outflow=0.15 cfs 0.027 af
Pond 4P: CB 12.0" Rou	Peak Elev=602.97' Inflow=0.01 cfs 0.003 af Ind Culvert n=0.013 L=21.0' S=0.0086 '/' Outflow=0.01 cfs 0.003 af
Pond 5P: CB 12.0" Rou	Peak Elev=601.65' Inflow=0.32 cfs 0.024 af and Culvert n=0.013 L=20.0' S=0.0100 '/' Outflow=0.32 cfs 0.024 af
Link 1L: Town System	Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af

Summary for Subcatchment 1S: Rear Parking & Northern Abutters

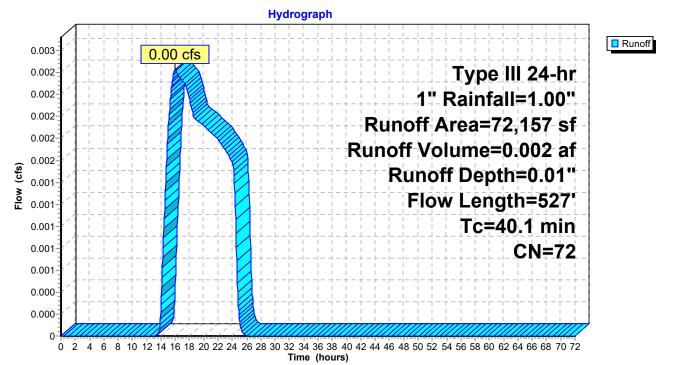
Runoff = 0.00 cfs @ 16.02 hrs, Volume= 0.002 af, Depth= 0.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1" Rainfall=1.00"

_	A	rea (sf)	CN	Description						
*		13,899	98	Paved Roa	Paved Road HSB B					
		12,683	69	50-75% Gra	ass cover, F	Fair, HSG B				
*		5,122	98	Buildings						
_		40,453	60	Woods, Fai	r, HSG B					
		72,157	72	Weighted A	verage					
		53,136		73.64% Per	rvious Area					
		19,021		26.36% Imp	pervious Are	ea				
	Tc	Length	Slop		Capacity	Description				
_	(min)	(feet)	(ft/ft	i) (ft/sec)	(cfs)					
	28.3	100	0.010	0.06		Sheet Flow, Sheet Flow				
						Woods: Light underbrush n= 0.400 P2= 3.20"				
	8.1	306	0.008	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow				
						Short Grass Pasture Kv= 7.0 fps				
	3.7	121	0.012	0 0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woods				
_						Woodland Kv= 5.0 fps				
	10 1	527	Total							

40.1 527 Total

Subcatchment 1S: Rear Parking & Northern Abutters



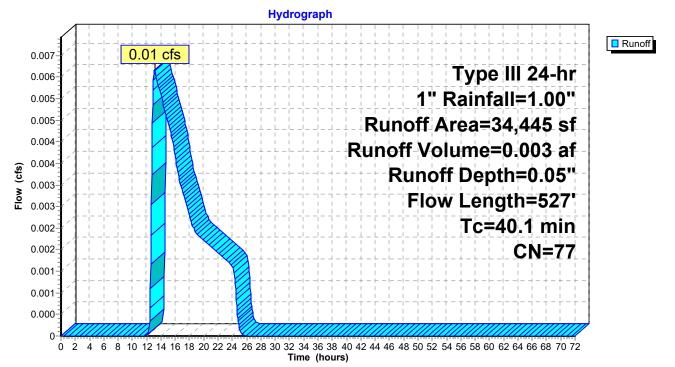
Summary for Subcatchment 2S: Side Driveways & Northern Abutters

Runoff = 0.01 cfs @ 13.13 hrs, Volume= 0.003 af, Depth= 0.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1" Rainfall=1.00"

_	A	rea (sf)	CN	Description						
*		7,619	98	Paved Road HSB B						
		12,149	69	50-75% Gra	50-75% Grass cover, Fair, HSG B					
*		5,055	98	Buildings						
_		9,622	60	Woods, Fai	r, HSG B					
		34,445	77	Weighted A	verage					
		21,771		63.21% Per	vious Area					
		12,674		36.79% Imp	pervious Are	ea				
	Тс	Length	Slope	e Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow				
						Woods: Light underbrush n= 0.400 P2= 3.20"				
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow				
						Short Grass Pasture Kv= 7.0 fps				
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woods				
_						Woodland Kv= 5.0 fps				
	40.1	527	Total							

Subcatchment 2S: Side Driveways & Northern Abutters



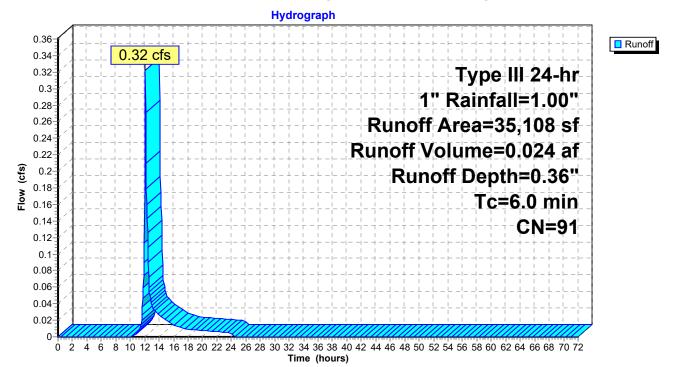
Summary for Subcatchment 3S: Buildings, Southern Parking, & Lawns

Runoff = 0.32 cfs @ 12.10 hrs, Volume= 0.024 af, Depth= 0.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1" Rainfall=1.00"

_	A	rea (sf)	CN	Description						
*		10,966	98	Paved Road HSB B						
		3,289	69	50-75% Grass cover, Fair, HSG B						
*		9,267	98	Buildings						
_		11,586	85	Gravel road	ls, HSG B					
		35,108	91	Weighted A	verage					
		14,875		42.37% Pervious Area						
		20,233	:	57.63% Impervious Area						
	Tc	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	6.0					Direct Entry, Direct Entry				





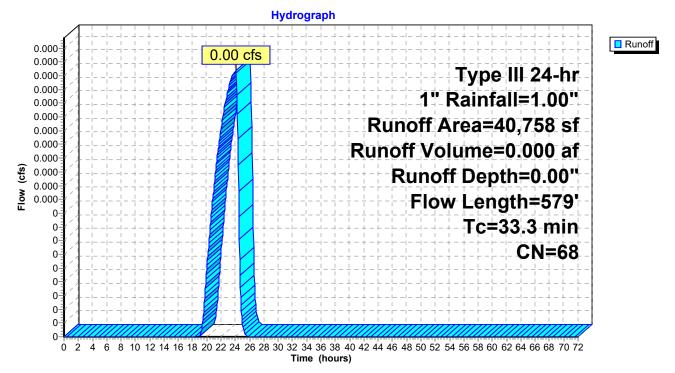
Summary for Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods

Runoff = 0.00 cfs @ 24.04 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1" Rainfall=1.00"

	A	rea (sf)	CN E	Description				
*		2,870	98 Paved Road HSB B					
		26,302	69 5	50-75% Gra	ass cover, F	Fair, HSG B		
*		0	98 E	Buildings				
		11,586	60 V	Voods, Fai	r, HSG B			
		40,758	68 V	Veighted A	verage			
		37,888	-		vious Area			
		2,870	7	'.04% Impe	ervious Area	а		
	_		~		a 14	-		
	Tc	Length	Slope		Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow		
						Woods: Light underbrush n= 0.400 P2= 3.20"		
	4.3	214	0.0140	0.83		Shallow Concentrated Flow, Shallow Concentrated Flow		
				~~ ~~		Short Grass Pasture Kv= 7.0 fps		
	0.1	100	0.1100	23.09	577.34	Channel Flow, Channel		
						Area= 25.0 sf Perim= 15.0' r= 1.67'		
	0.0	405	0 0000	4.05	405.00	n= 0.030 Earth, grassed & winding		
	0.6	165	0.0060	4.65	185.92	Channel Flow, Drain Channel		
						Area= 40.0 sf Perim= 30.0' r= 1.33'		
_						n= 0.030 Earth, grassed & winding		
	33.3	579	Total					

Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods



Summary for Pond 1P: SC-740 Storm Tech System - Rear

Inflow Area =	1.656 ac, 26.36% Impervious, Inflow De	epth = 0.01" for 1" event
Inflow =	0.00 cfs @ 16.02 hrs, Volume=	0.002 af
Outflow =	0.00 cfs @ 16.22 hrs, Volume=	0.002 af, Atten= 1%, Lag= 12.0 min
Discarded =	0.00 cfs @ 16.22 hrs, Volume=	0.002 af
Primary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 607.50' @ 16.22 hrs Surf.Area= 1,096 sf Storage= 1 cf

Plug-Flow detention time= 9.9 min calculated for 0.002 af (100% of inflow) Center-of-Mass det. time= 9.9 min (1,160.9 - 1,151.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	607.50'	1,020 cf	20.50'W x 53.46'L x 3.50'H Field A
			3,836 cf Overall - 1,286 cf Embedded = 2,549 cf x 40.0% Voids
#2A	608.00'	1,286 cf	ADS_StormTech SC-740 +Cap x 28 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			4 Rows of 7 Chambers
		2 306 cf	Total Available Storage

2,306 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	607.50'	1.020 in/hr Exfiltration over Surface area
#2	Primary	610.75'	5.0' long x 5.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88

Discarded OutFlow Max=0.03 cfs @ 16.22 hrs HW=607.50' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=607.50' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 1P: SC-740 Storm Tech System - Rear - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

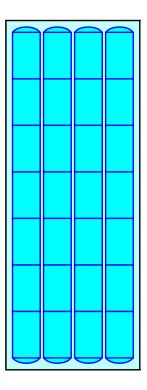
7 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 51.46' Row Length +12.0" End Stone x 2 = 53.46' Base Length 4 Rows x 51.0" Wide + 6.0" Spacing x 3 + 12.0" Side Stone x 2 = 20.50' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

28 Chambers x 45.9 cf = 1,286.3 cf Chamber Storage

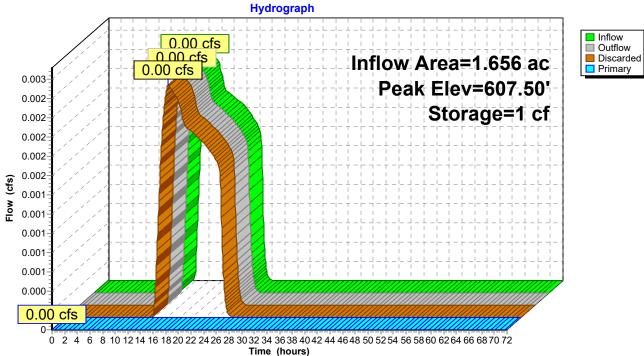
3,835.5 cf Field - 1,286.3 cf Chambers = 2,549.2 cf Stone x 40.0% Voids = 1,019.7 cf Stone Storage

Chamber Storage + Stone Storage = 2,306.0 cf = 0.053 afOverall Storage Efficiency = 60.1%Overall System Size = $53.46' \times 20.50' \times 3.50'$

28 Chambers 142.1 cy Field 94.4 cy Stone







Pond 1P: SC-740 Storm Tech System - Rear

Time (hours)

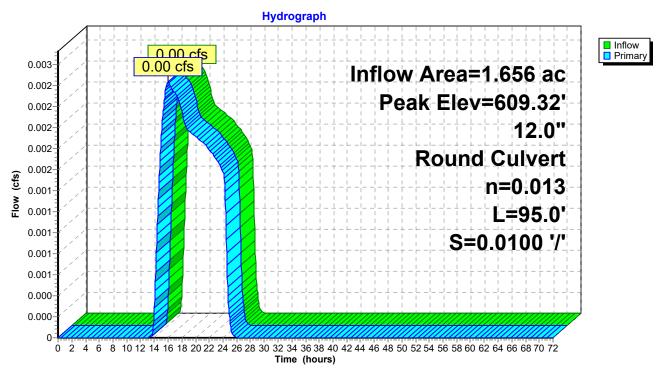
Summary for Pond 2P: CB

Inflow Area =	=	1.656 ac, 26.36% Impervious, Inf	low Depth = 0.01" for 1" event
Inflow =		0.00 cfs @ 16.02 hrs, Volume=	0.002 af
Outflow =		0.00 cfs @ 16.02 hrs, Volume=	0.002 af, Atten= 0%, Lag= 0.0 min
Primary =		0.00 cfs @ 16.02 hrs, Volume=	0.002 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 609.32' @ 16.02 hrs

Device F	Routing	Invert	Outlet Devices
	Primary	609.29'	12.0" Round Culvert L= 95.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 609.29' / 608.34' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 16.02 hrs HW=609.32' (Free Discharge) **1=Culvert** (Barrel Controls 0.00 cfs @ 0.63 fps)



Pond 2P: CB

Summary for Pond 3P: SC-740 Storm Tech System - Front

Inflow Area =	1.597 ac, 47.31% Impervious, Inflow Depth	= 0.21" for 1" event
Inflow =	0.32 cfs @ 12.10 hrs, Volume= 0.02	27 af
Outflow =	0.15 cfs @ 12.10 hrs, Volume= 0.02	27 af, Atten= 53%, Lag= 0.1 min
Discarded =	0.15 cfs @ 12.10 hrs, Volume= 0.02	27 af
Primary =	0.00 cfs @ 0.00 hrs, Volume= 0.00	00 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 600.56' @ 12.33 hrs Surf.Area= 6,372 sf Storage= 156 cf

Plug-Flow detention time= 11.5 min calculated for 0.027 af (100% of inflow) Center-of-Mass det. time= 11.3 min (886.7 - 875.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	600.50'	5,778 cf	92.75'W x 68.70'L x 3.50'H Field A
			22,301 cf Overall - 7,856 cf Embedded = 14,445 cf x 40.0% Voids
#2A	601.00'	7,856 cf	ADS_StormTech SC-740 +Cap x 171 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			19 Rows of 9 Chambers
		13 634 cf	Total Available Storage

13,634 cf Total Available Storage

Storage Group A created with Chamber Wizard

ar Weir
.60 1.80 2.00
5 2.65 2.65
١.

Discarded OutFlow Max=0.15 cfs @ 12.10 hrs HW=600.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.15 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=600.50' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 3P: SC-740 Storm Tech System - Front - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

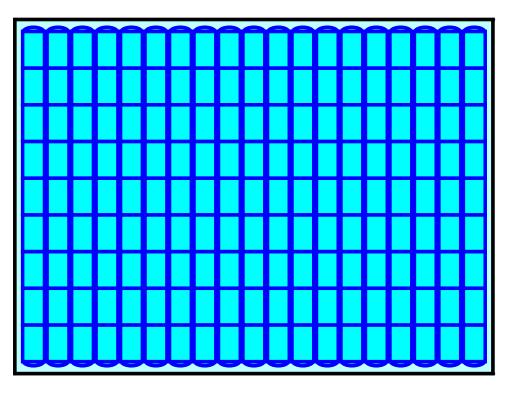
9 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 65.70' Row Length +18.0" End Stone x 2 = 68.70' Base Length 19 Rows x 51.0" Wide + 6.0" Spacing x 18 + 18.0" Side Stone x 2 = 92.75' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

171 Chambers x 45.9 cf = 7,855.7 cf Chamber Storage

22,300.7 cf Field - 7,855.7 cf Chambers = 14,444.9 cf Stone x 40.0% Voids = 5,778.0 cf Stone Storage

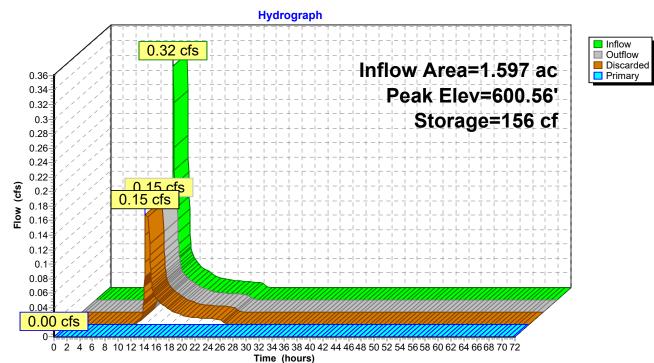
Chamber Storage + Stone Storage = 13,633.7 cf = 0.313 af Overall Storage Efficiency = 61.1% Overall System Size = 68.70' x 92.75' x 3.50'

171 Chambers 826.0 cy Field 535.0 cy Stone









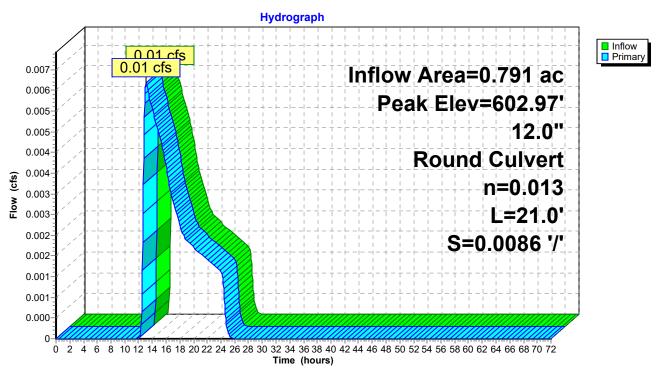
Summary for Pond 4P: CB

Inflow Area =	• 0.791 ac,	36.79% Impervious, In	nflow Depth = 0.05" for 1" event
Inflow =	0.01 cfs @	2 13.13 hrs, Volume=	0.003 af
Outflow =	0.01 cfs @	3.13 hrs, Volume=	0.003 af, Atten= 0%, Lag= 0.0 min
Primary =	0.01 cfs @) 13.13 hrs, Volume=	0.003 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 602.97' @ 13.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	602.93'	12.0" Round Culvert L= 21.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 602.93' / 602.75' S= 0.0086 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.01 cfs @ 13.13 hrs HW=602.97' (Free Discharge) **1=Culvert** (Barrel Controls 0.01 cfs @ 0.79 fps)



Pond 4P: CB

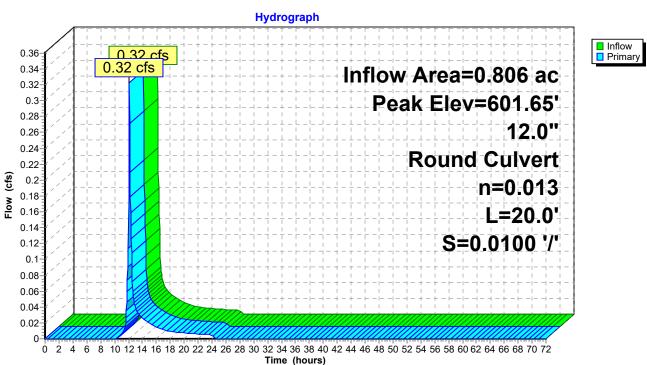
Summary for Pond 5P: CB

Inflow Area =	=	0.806 ac, 57.63% Impervious, Inflow	Depth = 0.36" for 1" event
Inflow =	:	0.32 cfs @ 12.10 hrs, Volume=	0.024 af
Outflow =	:	0.32 cfs @ 12.10 hrs, Volume=	0.024 af, Atten= 0%, Lag= 0.0 min
Primary =	:	0.32 cfs @ 12.10 hrs, Volume=	0.024 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 601.65' @ 12.10 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	601.33'	12.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 601.33' / 601.13' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.32 cfs @ 12.10 hrs HW=601.65' (Free Discharge) -1=Culvert (Inlet Controls 0.32 cfs @ 1.51 fps)

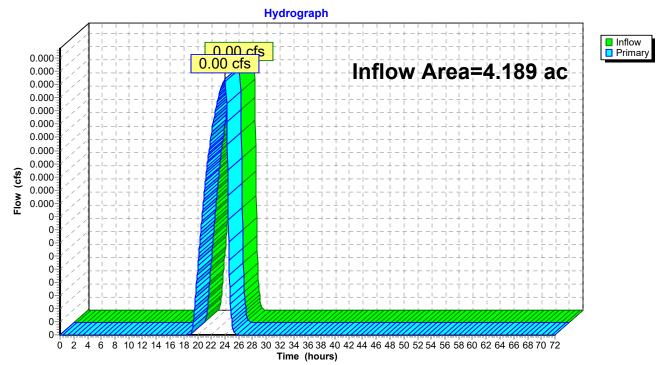


Pond 5P: CB

Summary for Link 1L: Town System

Inflow Area	a =	4.189 ac, 30.03% Impervious, Inflow Depth = 0.00" for 1" event
Inflow	=	0.00 cfs @ 24.04 hrs, Volume= 0.000 af
Primary	=	0.00 cfs $\overline{@}$ 24.04 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Link 1L: Town System

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Rear Parking &	Runoff Area=72,157 sf 26.36% Impervious Runoff Depth=0.89" Flow Length=527' Tc=40.1 min CN=72 Runoff=0.78 cfs 0.122 af
Subcatchment2S: Side Driveways &	Runoff Area=34,445 sf 36.79% Impervious Runoff Depth=1.16" Flow Length=527' Tc=40.1 min CN=77 Runoff=0.51 cfs 0.077 af
Subcatchment3S: Buildings, Southe	rn Runoff Area=35,108 sf 57.63% Impervious Runoff Depth=2.19" Tc=6.0 min CN=91 Runoff=2.00 cfs 0.147 af
Subcatchment4S: Access Driveways	s, Runoff Area=40,758 sf 7.04% Impervious Runoff Depth=0.69" Flow Length=579' Tc=33.3 min CN=68 Runoff=0.35 cfs 0.054 af
	1 - Rear Peak Elev=610.83' Storage=2,231 cf Inflow=0.78 cfs 0.122 af 0.03 cfs 0.078 af Primary=0.26 cfs 0.044 af Outflow=0.29 cfs 0.122 af
Pond 2P: CB 12.0"	Peak Elev=609.80' Inflow=0.78 cfs 0.122 af Round Culvert n=0.013 L=95.0' S=0.0100 '/' Outflow=0.78 cfs 0.122 af
	n - Front Peak Elev=601.68' Storage=4,775 cf Inflow=2.12 cfs 0.224 af 0.15 cfs 0.224 af Primary=0.00 cfs 0.000 af Outflow=0.15 cfs 0.224 af
Pond 4P: CB 12.0"	Peak Elev=603.34' Inflow=0.51 cfs 0.077 af Round Culvert n=0.013 L=21.0' S=0.0086 '/' Outflow=0.51 cfs 0.077 af
Pond 5P: CB 12.0"	Peak Elev=602.27' Inflow=2.00 cfs 0.147 af Round Culvert n=0.013 L=20.0' S=0.0100 '/' Outflow=2.00 cfs 0.147 af
Link 1L: Town System	Inflow=0.39 cfs 0.099 af Primary=0.39 cfs 0.099 af

Summary for Subcatchment 1S: Rear Parking & Northern Abutters

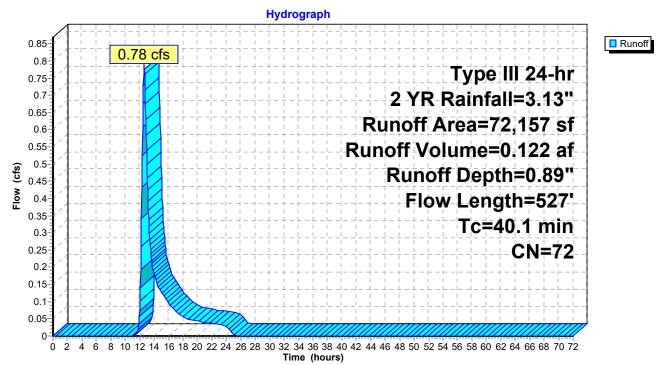
Runoff = 0.78 cfs @ 12.61 hrs, Volume= 0.122 af, Depth= 0.89"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YR Rainfall=3.13"

	А	rea (sf)	CN	Description		
*		13,899	98	Paved Road	d HSB B	
		12,683	69	50-75% Gra	ass cover, F	Fair, HSG B
*		5,122	98	Buildings		
		40,453	60	Woods, Fai	r, HSG B	
		72,157	72	Weighted A	verage	
		53,136		73.64% Per	rvious Area	l
		19,021		26.36% Imp	pervious Ar	ea
	Тс	Length	Slope	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft	t) (ft/sec)	(cfs)	
	28.3	100	0.0100	0 0.06		Sheet Flow, Sheet Flow
						Woods: Light underbrush n= 0.400 P2= 3.20"
	8.1	306	0.0080	0 0.63		Shallow Concentrated Flow, Shallow Concentrated Flow
						Short Grass Pasture Kv= 7.0 fps
	3.7	121	0.0120	0 0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woo
						Woodland Kv= 5.0 fps
	10.1	527	Total	-	-	

40.1 527 Total

Subcatchment 1S: Rear Parking & Northern Abutters



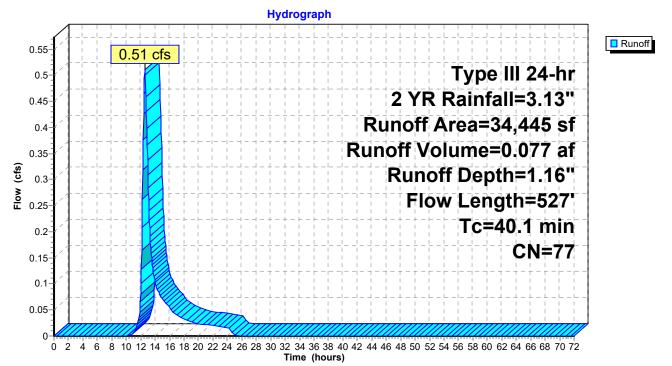
Summary for Subcatchment 2S: Side Driveways & Northern Abutters

Runoff = 0.51 cfs @ 12.59 hrs, Volume= 0.077 af, Depth= 1.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YR Rainfall=3.13"

_	A	rea (sf)	CN	Description		
*		7,619	98	Paved Road	d HSB B	
		12,149	69	50-75% Gra	ass cover, F	Fair, HSG B
*		5,055	98	Buildings		
_		9,622	60	Woods, Fai	r, HSG B	
		34,445	77	Weighted A	verage	
21,771 63.21% Pervious Area						
	12,674 36.79% Impervious Are				pervious Are	ea
	Тс	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow
						Woods: Light underbrush n= 0.400 P2= 3.20"
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow
						Short Grass Pasture Kv= 7.0 fps
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woods
_						Woodland Kv= 5.0 fps
	40.1	527	Total			

Subcatchment 2S: Side Driveways & Northern Abutters



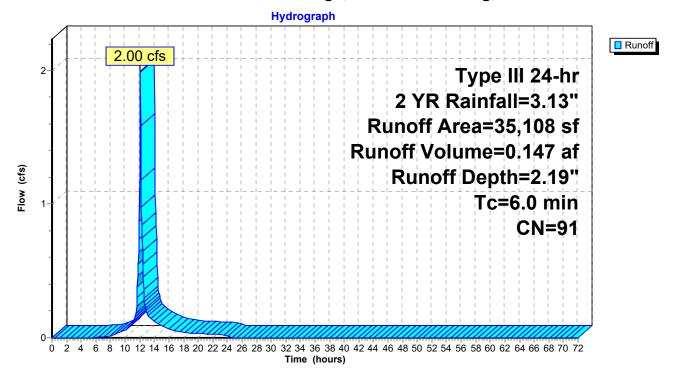
Summary for Subcatchment 3S: Buildings, Southern Parking, & Lawns

Runoff = 2.00 cfs @ 12.09 hrs, Volume= 0.147 af, Depth= 2.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YR Rainfall=3.13"

_	А	rea (sf)	CN	Description			
*		10,966	98	Paved Roa	d HSB B		
		3,289	69	50-75% Gra	ass cover, F	Fair, HSG B	
*		9,267	98	Buildings			
_		11,586	85	Gravel road	ls, HSG B		
		35,108	91	Weighted Average			
		14,875		42.37% Pervious Area			
		20,233		57.63% Imp	pervious Ar	ea	
	Tc	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	6.0					Direct Entry, Direct Entry	

Subcatchment 3S: Buildings, Southern Parking, & Lawns



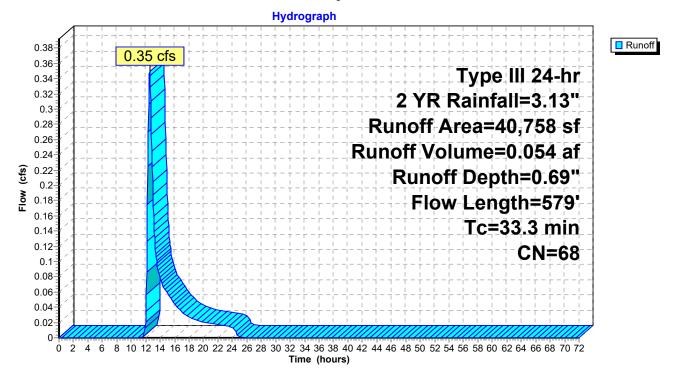
Summary for Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods

Runoff = 0.35 cfs @ 12.54 hrs, Volume= 0.054 af, Depth= 0.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YR Rainfall=3.13"

	A	rea (sf)	CN E	Description		
*		2,870	98 F	Paved Road	d HSB B	
		26,302	69 5	50-75% Gra	ass cover, F	Fair, HSG B
*		0		Buildings		
_		11,586	60 V	Voods, Fai	r, HSG B	
		40,758	68 V	Veighted A	verage	
		37,888	-		vious Area	
		2,870	7	'.04% Impe	ervious Area	a
	т.	1 11	0	V/.1	0	Description
	Tc (min)	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow
	4.0	044	0.0440	0.00		Woods: Light underbrush n= 0.400 P2= 3.20"
	4.3	214	0.0140	0.83		Shallow Concentrated Flow, Shallow Concentrated Flow
	0.1	100	0.1100	23.09	577.34	Short Grass Pasture Kv= 7.0 fps
	0.1	100	0.1100	23.09	577.54	Channel Flow, Channel Area= 25.0 sf Perim= 15.0' r= 1.67'
						n= 0.030 Earth, grassed & winding
	0.6	165	0.0060	4.65	185.92	Channel Flow, Drain Channel
	0.0	100	0.0000	1.00	100.02	Area= 40.0 sf Perim= 30.0' r= 1.33'
						n= 0.030 Earth, grassed & winding
_	33.3	579	Total			

Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods



Summary for Pond 1P: SC-740 Storm Tech System - Rear

Inflow Area =	1.656 ac, 26.36% Impervious, Inflow De	epth = 0.89" for 2 YR event
Inflow =	0.78 cfs @ 12.61 hrs, Volume=	0.122 af
Outflow =	0.29 cfs @ 13.38 hrs, Volume=	0.122 af, Atten= 63%, Lag= 46.2 min
Discarded =	0.03 cfs @ 11.95 hrs, Volume=	0.078 af
Primary =	0.26 cfs @ 13.38 hrs, Volume=	0.044 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 610.83' @ 13.38 hrs Surf.Area= 1,096 sf Storage= 2,231 cf

Plug-Flow detention time= 587.7 min calculated for 0.122 af (100% of inflow) Center-of-Mass det. time= 588.5 min (1,490.4 - 901.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	607.50'	1,020 cf	20.50'W x 53.46'L x 3.50'H Field A
			3,836 cf Overall - 1,286 cf Embedded = 2,549 cf x 40.0% Voids
#2A	608.00'	1,286 cf	ADS_StormTech SC-740 +Cap x 28 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			4 Rows of 7 Chambers
		2 306 cf	Total Available Storage

2,306 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	607.50'	1.020 in/hr Exfiltration over Surface area
#2	Primary	610.75'	5.0' long x 5.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88

Discarded OutFlow Max=0.03 cfs @ 11.95 hrs HW=607.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.26 cfs @ 13.38 hrs HW=610.83' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 0.26 cfs @ 0.66 fps)

Pond 1P: SC-740 Storm Tech System - Rear - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

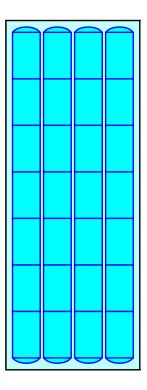
7 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 51.46' Row Length +12.0" End Stone x 2 = 53.46' Base Length 4 Rows x 51.0" Wide + 6.0" Spacing x 3 + 12.0" Side Stone x 2 = 20.50' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

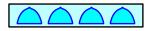
28 Chambers x 45.9 cf = 1,286.3 cf Chamber Storage

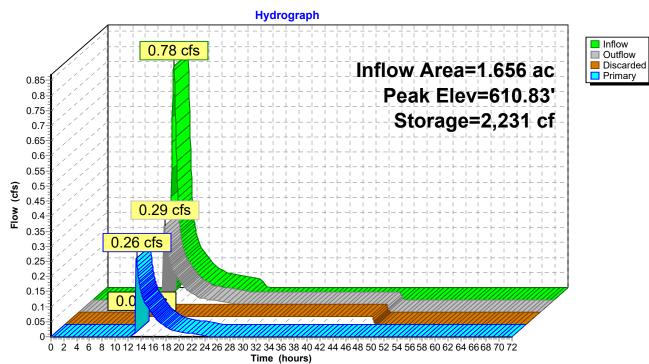
3,835.5 cf Field - 1,286.3 cf Chambers = 2,549.2 cf Stone x 40.0% Voids = 1,019.7 cf Stone Storage

Chamber Storage + Stone Storage = 2,306.0 cf = 0.053 afOverall Storage Efficiency = 60.1%Overall System Size = $53.46' \times 20.50' \times 3.50'$

28 Chambers 142.1 cy Field 94.4 cy Stone







Pond 1P: SC-740 Storm Tech System - Rear

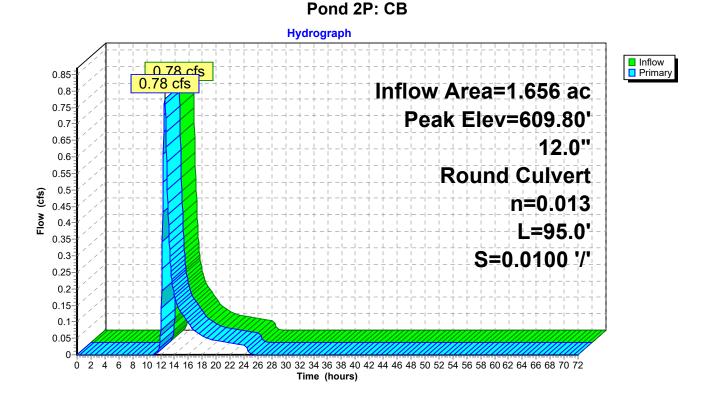
Summary for Pond 2P: CB

Inflow Area =	1.656 ac, 26.36% Impervious, Inflow I	Depth = 0.89" for 2 YR event
Inflow =	0.78 cfs @ 12.61 hrs, Volume=	0.122 af
Outflow =	0.78 cfs @ 12.61 hrs, Volume=	0.122 af, Atten= 0%, Lag= 0.0 min
Primary =	0.78 cfs @ 12.61 hrs, Volume=	0.122 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 609.80' @ 12.61 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	609.29'	12.0" Round Culvert L= 95.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 609.29' / 608.34' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.77 cfs @ 12.61 hrs HW=609.80' (Free Discharge) ☐ 1=Culvert (Inlet Controls 0.77 cfs @ 1.92 fps)



Summary for Pond 3P: SC-740 Storm Tech System - Front

Inflow Area =	1.597 ac, 47.31% Impervious, Inflow De	epth = 1.68" for 2 YR event
Inflow =	2.12 cfs @ 12.09 hrs, Volume=	0.224 af
Outflow =	0.15 cfs @ 11.40 hrs, Volume=	0.224 af, Atten= 93%, Lag= 0.0 min
Discarded =	0.15 cfs @ 11.40 hrs, Volume=	0.224 af
Primary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 601.68' @ 15.26 hrs Surf.Area= 6,372 sf Storage= 4,775 cf

Plug-Flow detention time= 310.1 min calculated for 0.224 af (100% of inflow) Center-of-Mass det. time= 310.0 min (1,141.4 - 831.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	600.50'	5,778 cf	92.75'W x 68.70'L x 3.50'H Field A
			22,301 cf Overall - 7,856 cf Embedded = 14,445 cf x 40.0% Voids
#2A	601.00'	7,856 cf	ADS_StormTech SC-740 +Cap x 171 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			19 Rows of 9 Chambers
		13 634 cf	Total Available Storage

13,634 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	600.50'	1.020 in/hr Exfiltration over Surface area
#2	Primary	603.90'	5.0' long x 5.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88

Discarded OutFlow Max=0.15 cfs @ 11.40 hrs HW=600.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.15 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=600.50' (Free Discharge) ←2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 3P: SC-740 Storm Tech System - Front - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

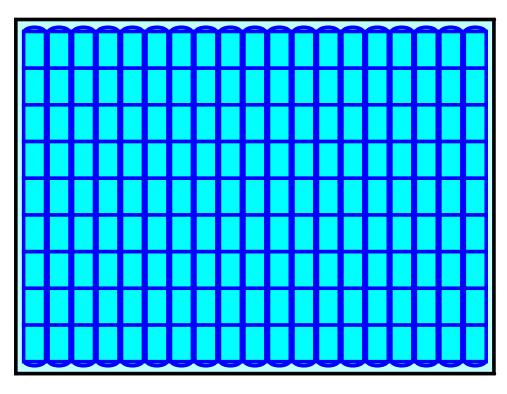
9 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 65.70' Row Length +18.0" End Stone x 2 = 68.70' Base Length 19 Rows x 51.0" Wide + 6.0" Spacing x 18 + 18.0" Side Stone x 2 = 92.75' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

171 Chambers x 45.9 cf = 7,855.7 cf Chamber Storage

22,300.7 cf Field - 7,855.7 cf Chambers = 14,444.9 cf Stone x 40.0% Voids = 5,778.0 cf Stone Storage

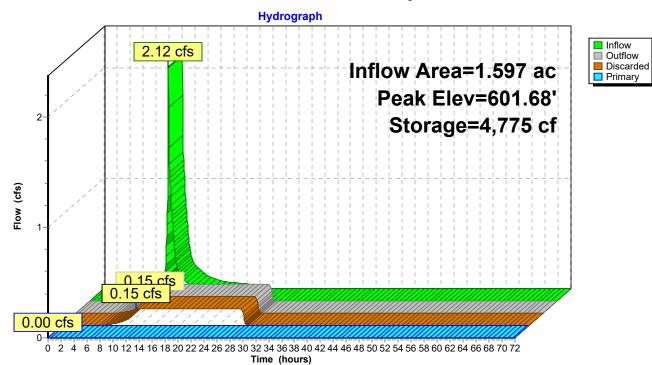
Chamber Storage + Stone Storage = 13,633.7 cf = 0.313 af Overall Storage Efficiency = 61.1% Overall System Size = 68.70' x 92.75' x 3.50'

171 Chambers 826.0 cy Field 535.0 cy Stone





Pond 3P: SC-740 Storm Tech System - Front



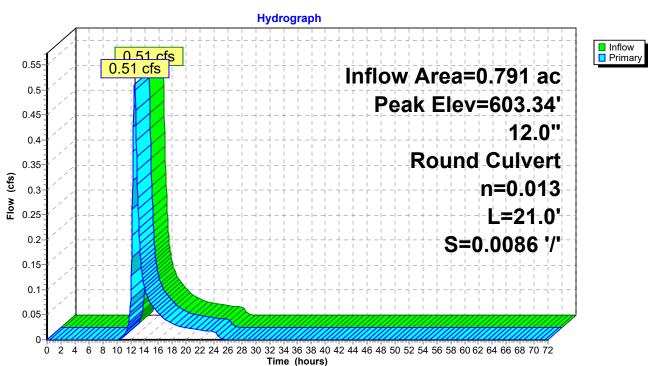
Summary for Pond 4P: CB

Inflow Area =	0.791 ac, 36.79% Impervious, Inflow I	Depth = 1.16" for 2 YR event
Inflow =	0.51 cfs @ 12.59 hrs, Volume=	0.077 af
Outflow =	0.51 cfs @ 12.59 hrs, Volume=	0.077 af, Atten= 0%, Lag= 0.0 min
Primary =	0.51 cfs @ 12.59 hrs, Volume=	0.077 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 603.34' @ 12.59 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	602.93'	12.0" Round Culvert L= 21.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 602.93' / 602.75' S= 0.0086 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.51 cfs @ 12.59 hrs HW=603.34' (Free Discharge) **1=Culvert** (Barrel Controls 0.51 cfs @ 2.48 fps)



Pond 4P: CB

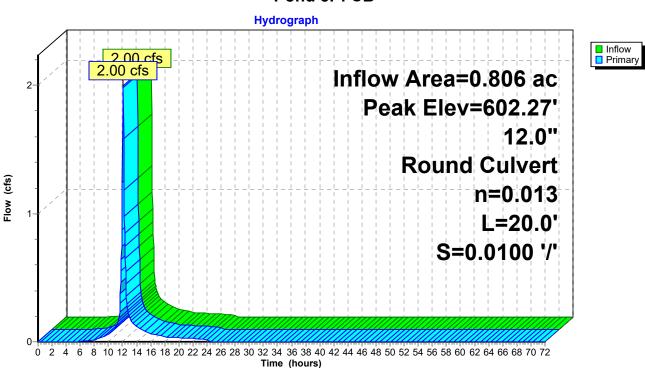
Summary for Pond 5P: CB

Inflow Area =	0.806 ac, 57.63% Impervious, Inflow D	epth = 2.19" for 2 YR event
Inflow =	2.00 cfs @ 12.09 hrs, Volume=	0.147 af
Outflow =	2.00 cfs @ 12.09 hrs, Volume=	0.147 af, Atten= 0%, Lag= 0.0 min
Primary =	2.00 cfs @ 12.09 hrs, Volume=	0.147 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 602.27' @ 12.09 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	601.33'	12.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 601.33' / 601.13' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.95 cfs @ 12.09 hrs HW=602.25' (Free Discharge)



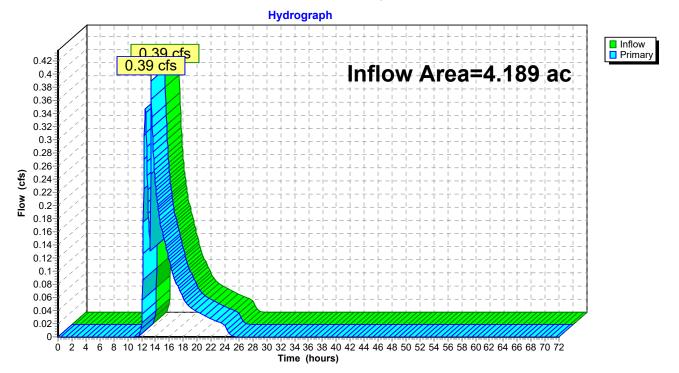
Pond 5P: CB

Summary for Link 1L: Town System

Inflow Area	=	4.189 ac, 30.03% Impervious, Inflow Depth = 0.28" for 2 YR event	
Inflow	=	0.39 cfs @ 13.37 hrs, Volume= 0.099 af	
Primary	=	0.39 cfs @ 13.37 hrs, Volume= 0.099 af, Atten= 0%, Lag= 0.0 min	

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 1L: Town System



Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Rear Parking &	Runoff Area=72,157 sf 26.36% Impervious Runoff Depth=1.92" Flow Length=527' Tc=40.1 min CN=72 Runoff=1.80 cfs 0.266 af
Subcatchment 2S: Side Driveways &	Runoff Area=34,445 sf 36.79% Impervious Runoff Depth=2.32" Flow Length=527' Tc=40.1 min CN=77 Runoff=1.05 cfs 0.153 af
Subcatchment3S: Buildings, Southern	Runoff Area=35,108 sf 57.63% Impervious Runoff Depth=3.63" Tc=6.0 min CN=91 Runoff=3.23 cfs 0.244 af
Subcatchment4S: Access Driveways,	Runoff Area=40,758 sf 7.04% Impervious Runoff Depth=1.63" Flow Length=579' Tc=33.3 min CN=68 Runoff=0.92 cfs 0.127 af
Pond 1P: SC-740 Storm Tech System - I Discarded=0.0	Rear Peak Elev=611.02' Storage=2,306 cf Inflow=1.80 cfs 0.266 af 3 cfs 0.081 af Primary=1.65 cfs 0.183 af Outflow=1.68 cfs 0.264 af
Pond 2P: CB 12.0" Rot	Peak Elev=610.15' Inflow=1.80 cfs 0.266 af und Culvert n=0.013 L=95.0' S=0.0100 '/' Outflow=1.80 cfs 0.266 af
Pond 3P: SC-740 Storm Tech System - Discarded=0.1	Peak Elev=602.92' Storage=10,478 cf Inflow=3.54 cfs 0.397 af 5 cfs 0.397 af Primary=0.00 cfs 0.000 af Outflow=0.15 cfs 0.397 af
Pond 4P: CB 12.0" Rot	Peak Elev=603.56' Inflow=1.05 cfs 0.153 af und Culvert n=0.013 L=21.0' S=0.0086 '/' Outflow=1.05 cfs 0.153 af
Pond 5P: CB 12.0" Rot	Peak Elev=603.00' Inflow=3.23 cfs 0.244 af und Culvert n=0.013 L=20.0' S=0.0100 '/' Outflow=3.23 cfs 0.244 af
Link 1L: Town System	Inflow=2.75 cfs 0.310 af Primary=2.75 cfs 0.310 af

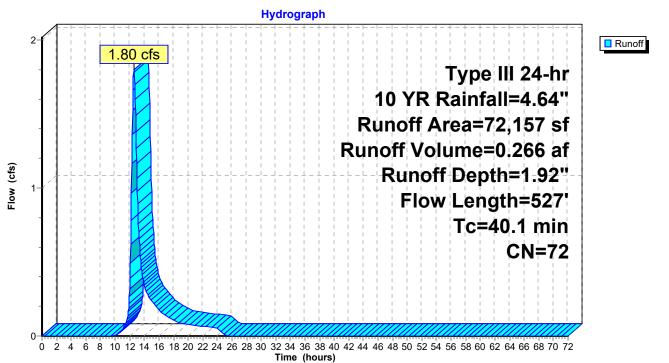
Summary for Subcatchment 1S: Rear Parking & Northern Abutters

Runoff = 1.80 cfs @ 12.58 hrs, Volume= 0.266 af, Depth= 1.92"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YR Rainfall=4.64"

_	A	rea (sf)	CN	Description					
*		13,899	98	Paved Roa	aved Road HSB B				
		12,683	69	50-75% Gra	ass cover, F	Fair, HSG B			
*		5,122	98	Buildings					
		40,453	60	Woods, Fai	r, HSG B				
		72,157	72	Weighted A	verage				
		53,136		73.64% Pei	rvious Area				
		19,021		26.36% Imp	pervious Are	ea			
	Тс	Length	Slope	e Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	·			
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow			
						Woods: Light underbrush n= 0.400 P2= 3.20"			
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow			
						Short Grass Pasture Kv= 7.0 fps			
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woods			
						Woodland Kv= 5.0 fps			
_	40.1	527	Total						

Subcatchment 1S: Rear Parking & Northern Abutters



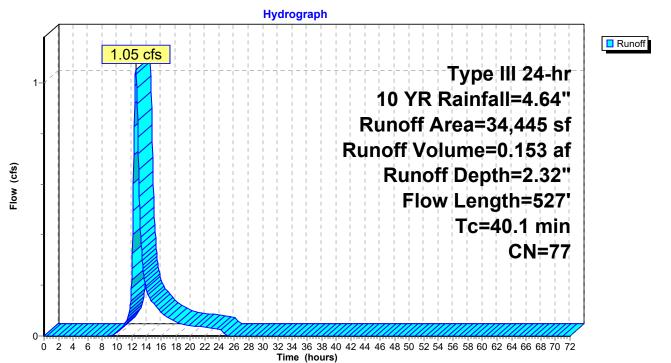
Summary for Subcatchment 2S: Side Driveways & Northern Abutters

Runoff = 1.05 cfs @ 12.57 hrs, Volume= 0.153 af, Depth= 2.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YR Rainfall=4.64"

_	A	rea (sf)	CN	Description					
*		7,619	98	Paved Road	ved Road HSB B				
		12,149	69	50-75% Gra	ass cover, F	Fair, HSG B			
*		5,055	98	Buildings					
_		9,622	60	Woods, Fai	r, HSG B				
		34,445	77	Weighted A	verage				
		21,771		63.21% Per	vious Area				
		12,674		36.79% Imp	pervious Ar	ea			
	Тс	Length	Slope		Capacity	Description			
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow			
						Woods: Light underbrush n= 0.400 P2= 3.20"			
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow			
						Short Grass Pasture Kv= 7.0 fps			
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woods			
_						Woodland Kv= 5.0 fps			
	40.1	527	Total						

Subcatchment 2S: Side Driveways & Northern Abutters

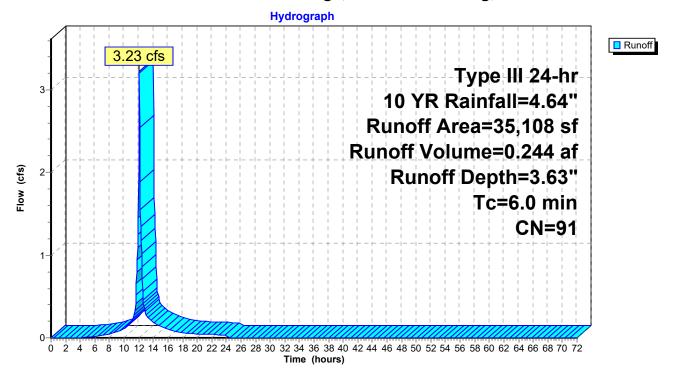


Runoff = 3.23 cfs @ 12.09 hrs, Volume= 0.244 af, Depth= 3.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YR Rainfall=4.64"

	A	rea (sf)	CN	Description				
*		10,966	98	Paved Roa	d HSB B			
		3,289	69	50-75% Gra	ass cover, l	Fair, HSG B		
*		9,267	98	Buildings				
		11,586	85	Gravel road	ls, HSG B			
		35,108	91	Weighted A	verage			
		14,875		42.37% Pe	rvious Area			
		20,233		57.63% Imp	pervious Ar	ea		
	Тс	Length	Slope		Capacity	Description		
(m	nin)	(feet)	(ft/ft) (ft/sec)	(cfs)			
(6.0					Direct Entry, Direct Entry		

Subcatchment 3S: Buildings, Southern Parking, & Lawns



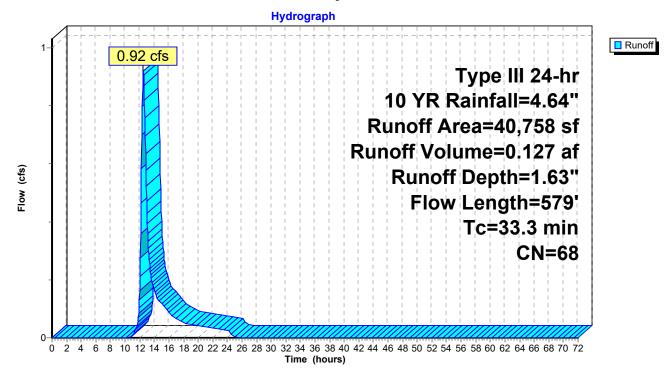
Summary for Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods

Runoff = 0.92 cfs @ 12.50 hrs, Volume= 0.127 af, Depth= 1.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YR Rainfall=4.64"

_	A	rea (sf)	CN E	Description			
*		2,870	98 F	98 Paved Road HSB B			
		26,302	69 5	50-75% Gra	ass cover, F	Fair, HSG B	
*		0	98 E	Buildings			
_		11,586	60 V	Voods, Fai	r, HSG B		
		40,758	68 V	Veighted A	verage		
		37,888	-		rvious Area		
		2,870	7	'.04% Impe	ervious Area	a	
	–	1 11.	0	V/.1	0	Description	
	Tc (min)	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	<u>(ft/ft)</u>	(ft/sec)	(cfs)		
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow	
	4.0	044	0 04 40	0.00		Woods: Light underbrush n= 0.400 P2= 3.20"	
	4.3	214	0.0140	0.83		Shallow Concentrated Flow, Shallow Concentrated Flow	
	0.1	100	0.1100	23.09	577.34	Short Grass Pasture Kv= 7.0 fps Channel Flow, Channel	
	0.1	100	0.1100	23.09	577.54	Area= 25.0 sf Perim= 15.0' r= 1.67'	
						n= 0.030 Earth, grassed & winding	
	0.6	165	0.0060	4.65	185.92	Channel Flow, Drain Channel	
	0.0	100	0.0000	1.00	100.02	Area= 40.0 sf Perim= 30.0' r= 1.33'	
						n= 0.030 Earth, grassed & winding	
_	33.3	579	Total				

Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods



Summary for Pond 1P: SC-740 Storm Tech System - Rear

Inflow Area =	1.656 ac, 26.36% Impervious, Inflow D	epth = 1.92" for 10 YR event
Inflow =	1.80 cfs @ 12.58 hrs, Volume=	0.266 af
Outflow =	1.68 cfs @_ 12.58 hrs, Volume=	0.264 af, Atten= 7%, Lag= 0.0 min
Discarded =	0.03 cfs @10.90 hrs, Volume=	0.081 af
Primary =	1.65 cfs @ 12.58 hrs, Volume=	0.183 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 611.02' @ 12.60 hrs Surf.Area= 1,096 sf Storage= 2,306 cf

Plug-Flow detention time= 284.5 min calculated for 0.264 af (100% of inflow) Center-of-Mass det. time= 281.5 min (1,159.5 - 878.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	607.50'	1,020 cf	20.50'W x 53.46'L x 3.50'H Field A
			3,836 cf Overall - 1,286 cf Embedded = 2,549 cf x 40.0% Voids
#2A	608.00'	1,286 cf	ADS_StormTech SC-740 +Cap x 28 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			4 Rows of 7 Chambers
		2 306 cf	Total Available Storage

2,306 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	607.50'	1.020 in/hr Exfiltration over Surface area
#2	Primary	610.75'	5.0' long x 5.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88

Discarded OutFlow Max=0.03 cfs @ 10.90 hrs HW=607.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=1.64 cfs @ 12.58 hrs HW=611.02' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 1.64 cfs @ 1.24 fps)

Pond 1P: SC-740 Storm Tech System - Rear - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

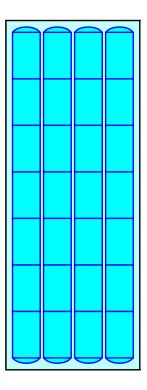
7 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 51.46' Row Length +12.0" End Stone x 2 = 53.46' Base Length 4 Rows x 51.0" Wide + 6.0" Spacing x 3 + 12.0" Side Stone x 2 = 20.50' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

28 Chambers x 45.9 cf = 1,286.3 cf Chamber Storage

3,835.5 cf Field - 1,286.3 cf Chambers = 2,549.2 cf Stone x 40.0% Voids = 1,019.7 cf Stone Storage

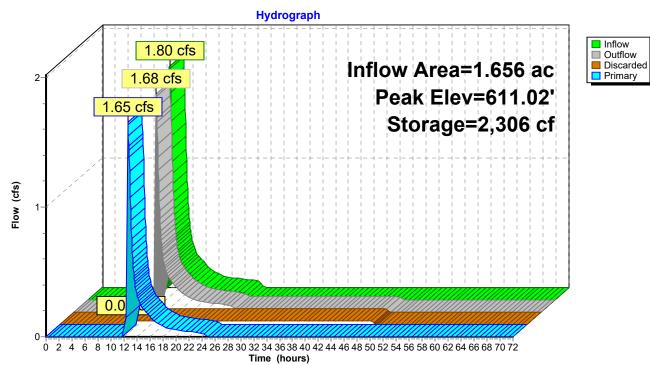
Chamber Storage + Stone Storage = 2,306.0 cf = 0.053 afOverall Storage Efficiency = 60.1%Overall System Size = $53.46' \times 20.50' \times 3.50'$

28 Chambers 142.1 cy Field 94.4 cy Stone









Summary for Pond 2P: CB

 Inflow Area =
 1.656 ac, 26.36% Impervious, Inflow Depth =
 1.92" for 10 YR event

 Inflow =
 1.80 cfs @
 12.58 hrs, Volume=
 0.266 af

 Outflow =
 1.80 cfs @
 12.58 hrs, Volume=
 0.266 af, Atten= 0%, Lag= 0.0 min

 Primary =
 1.80 cfs @
 12.58 hrs, Volume=
 0.266 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 610.15' @ 12.58 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	609.29'	12.0" Round Culvert L= 95.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 609.29' / 608.34' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.80 cfs @ 12.58 hrs HW=610.15' (Free Discharge)

Pond 2P: CB Hydrograph Inflow 1 80 cfs 2 Primary 1.80 cfs Inflow Area=1.656 ac Peak Elev=610.15' 12.0" **Round Culvert** Flow (cfs) n=0.013 L=95.0' S=0.0100 '/' 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

Summary for Pond 3P: SC-740 Storm Tech System - Front

Inflow Area =	1.597 ac, 47.31% Impervious, Inflow De	epth = 2.99" for 10 YR event
Inflow =	3.54 cfs @ 12.09 hrs, Volume=	0.397 af
Outflow =	0.15 cfs @ 10.40 hrs, Volume=	0.397 af, Atten= 96%, Lag= 0.0 min
Discarded =	0.15 cfs @ 10.40 hrs, Volume=	0.397 af
Primary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 602.92' @ 16.95 hrs Surf.Area= 6,372 sf Storage= 10,478 cf

Plug-Flow detention time= 660.2 min calculated for 0.397 af (100% of inflow) Center-of-Mass det. time= 660.4 min (1,478.9 - 818.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	600.50'	5,778 cf	92.75'W x 68.70'L x 3.50'H Field A
			22,301 cf Overall - 7,856 cf Embedded = 14,445 cf x 40.0% Voids
#2A	601.00'	7,856 cf	ADS_StormTech SC-740 +Cap x 171 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			19 Rows of 9 Chambers
		13 634 cf	Total Available Storage

13,634 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	600.50'	1.020 in/hr Exfiltration over Surface area
#2	Primary	603.90'	5.0' long x 5.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88

Discarded OutFlow Max=0.15 cfs @ 10.40 hrs HW=600.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.15 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=600.50' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 3P: SC-740 Storm Tech System - Front - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

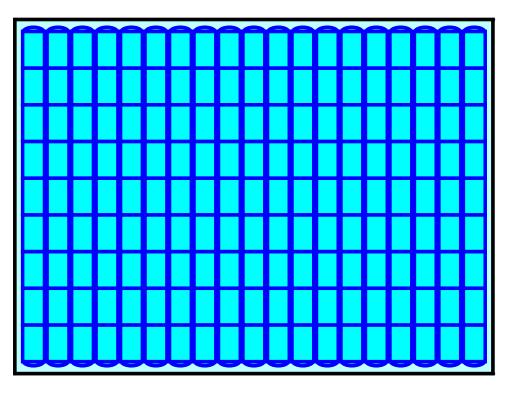
9 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 65.70' Row Length +18.0" End Stone x 2 = 68.70' Base Length 19 Rows x 51.0" Wide + 6.0" Spacing x 18 + 18.0" Side Stone x 2 = 92.75' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

171 Chambers x 45.9 cf = 7,855.7 cf Chamber Storage

22,300.7 cf Field - 7,855.7 cf Chambers = 14,444.9 cf Stone x 40.0% Voids = 5,778.0 cf Stone Storage

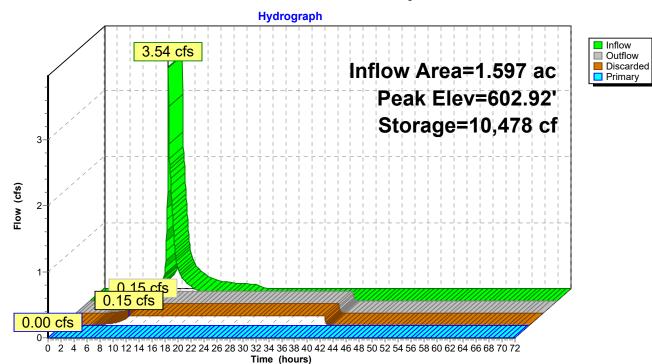
Chamber Storage + Stone Storage = 13,633.7 cf = 0.313 af Overall Storage Efficiency = 61.1% Overall System Size = 68.70' x 92.75' x 3.50'

171 Chambers 826.0 cy Field 535.0 cy Stone





Pond 3P: SC-740 Storm Tech System - Front



Summary for Pond 4P: CB

 Inflow Area =
 0.791 ac, 36.79% Impervious, Inflow Depth =
 2.32" for 10 YR event

 Inflow =
 1.05 cfs @
 12.57 hrs, Volume=
 0.153 af

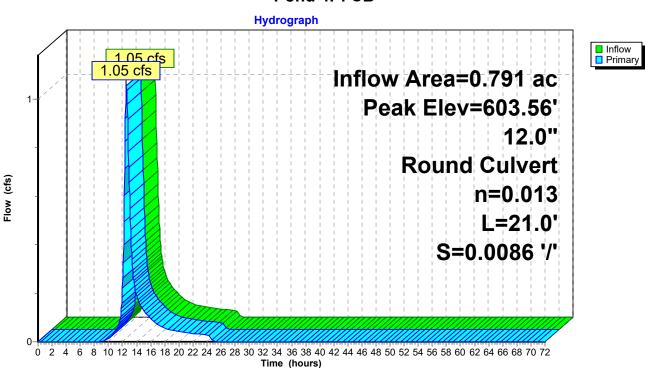
 Outflow =
 1.05 cfs @
 12.57 hrs, Volume=
 0.153 af, Atten= 0%, Lag= 0.0 min

 Primary =
 1.05 cfs @
 12.57 hrs, Volume=
 0.153 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 603.56' @ 12.57 hrs

Device	Routing	Invert	Outlet Devices
	Primary	602.93'	12.0" Round Culvert L= 21.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 602.93' / 602.75' S= 0.0086 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.05 cfs @ 12.57 hrs HW=603.56' (Free Discharge) —1=Culvert (Barrel Controls 1.05 cfs @ 2.89 fps)



Pond 4P: CB

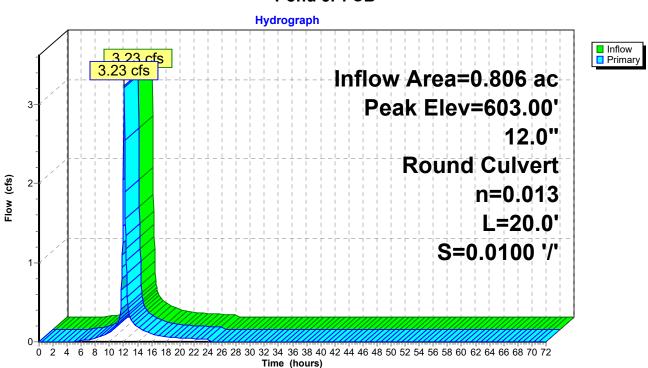
Summary for Pond 5P: CB

Inflow Area =	0.806 ac, 57.63% Impervious, Inflow De	epth = 3.63" for 10 YR event
Inflow =	3.23 cfs @ 12.09 hrs, Volume=	0.244 af
Outflow =	3.23 cfs @ 12.09 hrs, Volume=	0.244 af, Atten= 0%, Lag= 0.0 min
Primary =	3.23 cfs @ 12.09 hrs, Volume=	0.244 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 603.00' @ 12.09 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	601.33'	12.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 601.33' / 601.13' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=3.15 cfs @ 12.09 hrs HW=602.94' (Free Discharge) **1=Culvert** (Inlet Controls 3.15 cfs @ 4.01 fps)



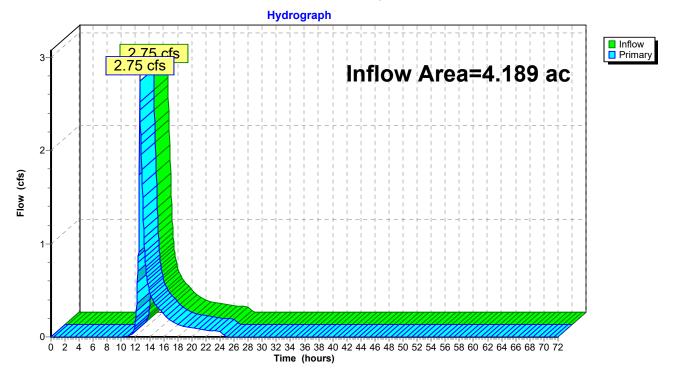
Pond 5P: CB

Summary for Link 1L: Town System

Inflow Area =	4.189 ac,	30.03% Impervious,	Inflow Depth = 0.8	9" for 10 YR event
Inflow =	2.75 cfs @	2 12.57 hrs, Volume	= 0.310 af	
Primary =	2.75 cfs @	2 12.57 hrs, Volume	= 0.310 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 1L: Town System



Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Rear Parking &	Runoff Area=72,157 sf 26.36% Impervious Runoff Depth=2.84" Flow Length=527' Tc=40.1 min CN=72 Runoff=2.69 cfs 0.392 af
Subcatchment 2S: Side Driveways &	Runoff Area=34,445 sf 36.79% Impervious Runoff Depth=3.31" Flow Length=527' Tc=40.1 min CN=77 Runoff=1.51 cfs 0.218 af
Subcatchment3S: Buildings, Southern	Runoff Area=35,108 sf 57.63% Impervious Runoff Depth=4.77" Tc=6.0 min CN=91 Runoff=4.18 cfs 0.320 af
Subcatchment4S: Access Driveways,	Runoff Area=40,758 sf 7.04% Impervious Runoff Depth=2.48" Flow Length=579' Tc=33.3 min CN=68 Runoff=1.44 cfs 0.193 af
Pond 1P: SC-740 Storm Tech System - Discarded=0.0	Rear Peak Elev=611.06' Storage=2,306 cf Inflow=2.69 cfs 0.392 af 3 cfs 0.083 af Primary=2.09 cfs 0.282 af Outflow=2.11 cfs 0.365 af
Pond 2P: CB 12.0" Ro	Peak Elev=610.60' Inflow=2.69 cfs 0.392 af und Culvert n=0.013 L=95.0' S=0.0100 '/' Outflow=2.69 cfs 0.392 af
Pond 3P: SC-740 Storm Tech System - Discarded=0.1	Peak Elev=603.99' Storage=13,603 cf Inflow=4.66 cfs 0.539 af 5 cfs 0.489 af Primary=0.31 cfs 0.050 af Outflow=0.46 cfs 0.539 af
Pond 4P: CB 12.0" Ro	Peak Elev=603.72' Inflow=1.51 cfs 0.218 af und Culvert n=0.013 L=21.0' S=0.0086 '/' Outflow=1.51 cfs 0.218 af
Pond 5P: CB 12.0" Ro	Peak Elev=603.78' Inflow=4.18 cfs 0.320 af und Culvert n=0.013 L=20.0' S=0.0100 '/' Outflow=4.18 cfs 0.320 af
Link 1L: Town System	Inflow=3.49 cfs 0.525 af Primary=3.49 cfs 0.525 af

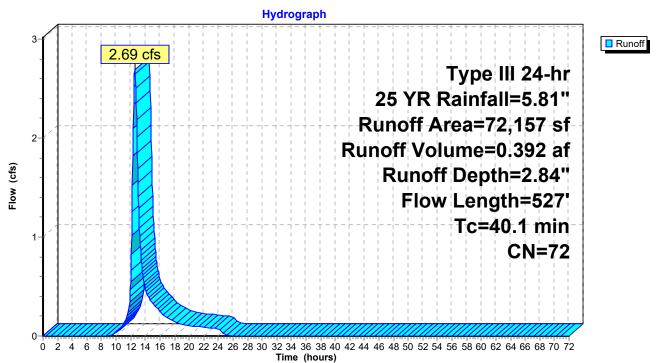
Summary for Subcatchment 1S: Rear Parking & Northern Abutters

Runoff = 2.69 cfs @ 12.57 hrs, Volume= 0.392 af, Depth= 2.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YR Rainfall=5.81"

_	A	rea (sf)	CN	Description						
*		13,899	98	Paved Road	aved Road HSB B					
		12,683	69	50-75% Gra	ass cover, F	Fair, HSG B				
*		5,122	98	Buildings						
		40,453	60	Woods, Fai	r, HSG B					
		72,157	72	Weighted A	verage					
		53,136		73.64% Per	rvious Area					
		19,021		26.36% Imp	pervious Ar	ea				
				-						
	Тс	Length	Slope	e Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow				
						Woods: Light underbrush n= 0.400 P2= 3.20"				
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow				
						Short Grass Pasture Kv= 7.0 fps				
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woods				
_						Woodland Kv= 5.0 fps				
-	40.1	527	Total							

Subcatchment 1S: Rear Parking & Northern Abutters



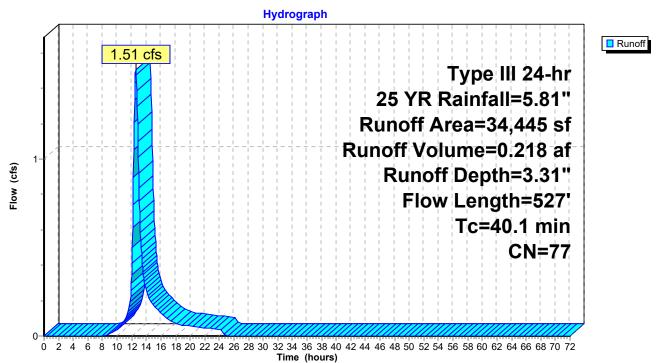
Summary for Subcatchment 2S: Side Driveways & Northern Abutters

Runoff = 1.51 cfs @ 12.56 hrs, Volume= 0.218 af, Depth= 3.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YR Rainfall=5.81"

	A	rea (sf)	CN	Description					
*		7,619	98	Paved Road	Paved Road HSB B				
		12,149	69	50-75% Gra	50-75% Grass cover, Fair, HSG B				
*		5,055	98	Buildings					
_		9,622	60	Woods, Fai	r, HSG B				
		34,445	77	Weighted A	verage				
		21,771		63.21% Per	vious Area				
		12,674		36.79% Imp	pervious Are	ea			
	Тс	Length	Slope	e Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow			
						Woods: Light underbrush n= 0.400 P2= 3.20"			
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow			
						Short Grass Pasture Kv= 7.0 fps			
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woods			
_						Woodland Kv= 5.0 fps			
	40.1	527	Total						

Subcatchment 2S: Side Driveways & Northern Abutters



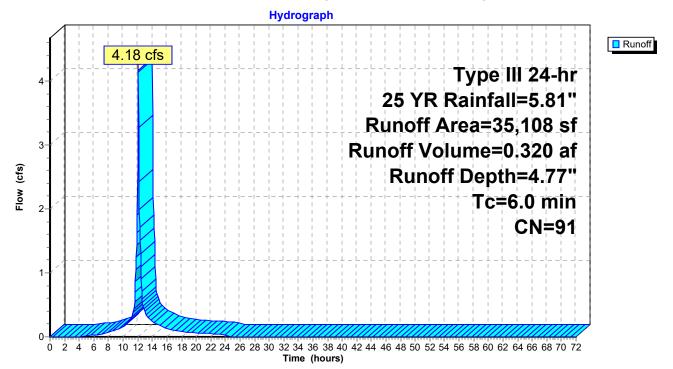
Summary for Subcatchment 3S: Buildings, Southern Parking, & Lawns

Runoff = 4.18 cfs @ 12.09 hrs, Volume= 0.320 af, Depth= 4.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YR Rainfall=5.81"

A	rea (sf)	CN	Description				
	10,966	98	Paved Roa	d HSB B			
	3,289	69	50-75% Gra	ass cover, l	Fair, HSG B		
	9,267	98	Buildings				
	11,586	85	Gravel road	ls, HSG B			
	35,108	91	Weighted A	verage			
	14,875		42.37% Pei	vious Area			
	20,233		57.63% Imp	pervious Ar	ea		
Тс	Length		,	Capacity	Description		
min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
6.0					Direct Entry, Direct Entry		
	Tc nin)	3,289 9,267 11,586 35,108 14,875 20,233 Tc Length nin) (feet)	10,966 98 3,289 69 9,267 98 11,586 85 35,108 91 14,875 4 20,233 5 Tc Length Slope nin) (feet) (ft/ft)	10,966 98 Paved Road 3,289 69 50-75% Gravel 9,267 98 Buildings 11,586 85 Gravel road 35,108 91 Weighted A 14,875 42.37% Per 20,233 57.63% Imp Tc Length Slope Velocity nin) (feet) (ft/ft) (ft/sec)	10,96698Paved Road HSB B3,2896950-75% Grass cover, I9,26798Buildings11,58685Gravel roads, HSG B35,10891Weighted Average14,87542.37% Pervious Area20,23357.63% Impervious ArTcLengthSlopeVelocityNin)(feet)(ft/ft)(ft/sec)		





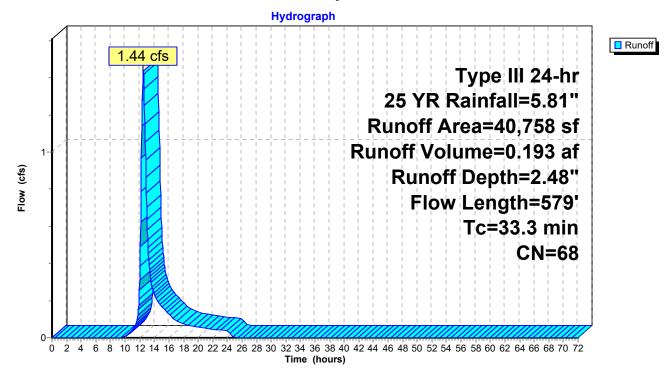
Summary for Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods

Runoff = 1.44 cfs @ 12.48 hrs, Volume= 0.193 af, Depth= 2.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YR Rainfall=5.81"

	A	rea (sf)	CN [Description			
*		2,870	98 F	98 Paved Road HSB B			
		26,302	69 5	50-75% Gra	ass cover, F	Fair, HSG B	
*		0		Buildings			
_		11,586	<u>60 \</u>	Voods, Fai	r, HSG B		
		40,758	68 \	Veighted A	verage		
		37,888	-		rvious Area		
		2,870	7	7.04% Impe	ervious Area	a	
	т.	1	0	M. L	0	Description	
	Tc (min)	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	<u>(ft/ft)</u>	(ft/sec)	(cfs)		
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow	
	4.0	044	0.04.40	0.00		Woods: Light underbrush n= 0.400 P2= 3.20"	
	4.3	214	0.0140	0.83		Shallow Concentrated Flow, Shallow Concentrated Flow	
	0.1	100	0.1100	23.09	577.34	Short Grass Pasture Kv= 7.0 fps	
	0.1	100	0.1100	23.09	577.54	Channel Flow, Channel Area= 25.0 sf Perim= 15.0' r= 1.67'	
						n = 0.030 Earth, grassed & winding	
	0.6	165	0.0060	4.65	185.92	Channel Flow, Drain Channel	
	0.0	100	0.0000	4.00	100.02	Area= 40.0 sf Perim= 30.0' r= 1.33'	
						n= 0.030 Earth, grassed & winding	
	33.3	579	Total				

Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods



Summary for Pond 1P: SC-740 Storm Tech System - Rear

Inflow Area =	1.656 ac, 26.36% Impervious, Inflow De	epth = 2.84" for 25 YR event
Inflow =	2.69 cfs @ 12.57 hrs, Volume=	0.392 af
Outflow =	2.11 cfs @ 12.57 hrs, Volume=	0.365 af, Atten= 22%, Lag= 0.0 min
Discarded =	0.03 cfs @ 10.05 hrs, Volume=	0.083 af
Primary =	2.09 cfs $\overline{@}$ 12.57 hrs, Volume=	0.282 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 611.06' @ 12.57 hrs Surf.Area= 1,096 sf Storage= 2,306 cf

Plug-Flow detention time= 249.7 min calculated for 0.365 af (93% of inflow) Center-of-Mass det. time= 215.0 min (1,081.7 - 866.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	607.50'	1,020 cf	20.50'W x 53.46'L x 3.50'H Field A
			3,836 cf Overall - 1,286 cf Embedded = 2,549 cf x 40.0% Voids
#2A	608.00'	1,286 cf	ADS_StormTech SC-740 +Cap x 28 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			4 Rows of 7 Chambers
		2 306 cf	Total Available Storage

2,306 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	607.50'	1.020 in/hr Exfiltration over Surface area
#2	Primary	610.75'	5.0' long x 5.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88

Discarded OutFlow Max=0.03 cfs @ 10.05 hrs HW=607.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=2.08 cfs @ 12.57 hrs HW=611.06' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 2.08 cfs @ 1.35 fps)

Pond 1P: SC-740 Storm Tech System - Rear - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

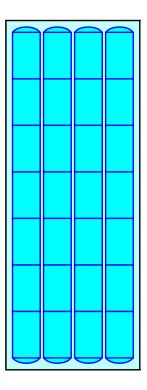
7 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 51.46' Row Length +12.0" End Stone x 2 = 53.46' Base Length 4 Rows x 51.0" Wide + 6.0" Spacing x 3 + 12.0" Side Stone x 2 = 20.50' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

28 Chambers x 45.9 cf = 1,286.3 cf Chamber Storage

3,835.5 cf Field - 1,286.3 cf Chambers = 2,549.2 cf Stone x 40.0% Voids = 1,019.7 cf Stone Storage

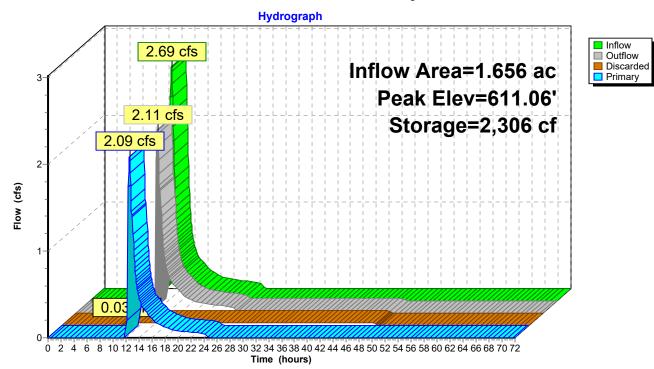
Chamber Storage + Stone Storage = 2,306.0 cf = 0.053 afOverall Storage Efficiency = 60.1%Overall System Size = $53.46' \times 20.50' \times 3.50'$

28 Chambers 142.1 cy Field 94.4 cy Stone





Pond 1P: SC-740 Storm Tech System - Rear



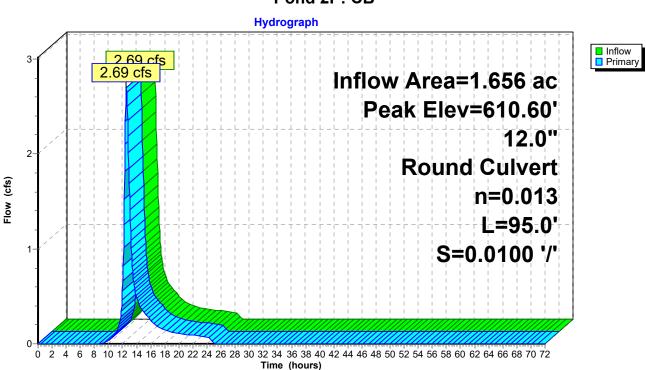
Summary for Pond 2P: CB

Inflow Area =	1.656 ac, 26.36% Impervious, Inflow D	epth = 2.84" for 25 YR event
Inflow =	2.69 cfs @ 12.57 hrs, Volume=	0.392 af
Outflow =	2.69 cfs @ 12.57 hrs, Volume=	0.392 af, Atten= 0%, Lag= 0.0 min
Primary =	2.69 cfs @ 12.57 hrs, Volume=	0.392 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 610.60' @ 12.57 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	609.29'	12.0" Round Culvert L= 95.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 609.29' / 608.34' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.69 cfs @ 12.57 hrs HW=610.60' (Free Discharge) -1=Culvert (Inlet Controls 2.69 cfs @ 3.42 fps)



Pond 2P: CB

Summary for Pond 3P: SC-740 Storm Tech System - Front

Inflow Area =	1.597 ac, 47.31% Impervious, Inflow De	epth = 4.05" for 25 YR event
Inflow =	4.66 cfs @ 12.09 hrs, Volume=	0.539 af
Outflow =	0.46 cfs @ 14.14 hrs, Volume=	0.539 af, Atten= 90%, Lag= 122.7 min
Discarded =	0.15 cfs @ 9.60 hrs, Volume=	0.489 af
Primary =	0.31 cfs $\overline{@}$ 14.14 hrs, Volume=	0.050 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 603.99' @ 14.14 hrs Surf.Area= 6,372 sf Storage= 13,603 cf

Plug-Flow detention time= 768.2 min calculated for 0.538 af (100% of inflow) Center-of-Mass det. time= 768.7 min (1,580.1 - 811.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	600.50'	5,778 cf	92.75'W x 68.70'L x 3.50'H Field A
			22,301 cf Overall - 7,856 cf Embedded = 14,445 cf x 40.0% Voids
#2A	601.00'	7,856 cf	ADS_StormTech SC-740 +Cap x 171 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			19 Rows of 9 Chambers
		13 634 cf	Total Available Storage

13,634 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	600.50'	1.020 in/hr Exfiltration over Surface area
#2	Primary	603.90'	5.0' long x 5.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88

Discarded OutFlow Max=0.15 cfs @ 9.60 hrs HW=600.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.15 cfs)

Primary OutFlow Max=0.31 cfs @ 14.14 hrs HW=603.99' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 0.31 cfs @ 0.69 fps)

Pond 3P: SC-740 Storm Tech System - Front - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

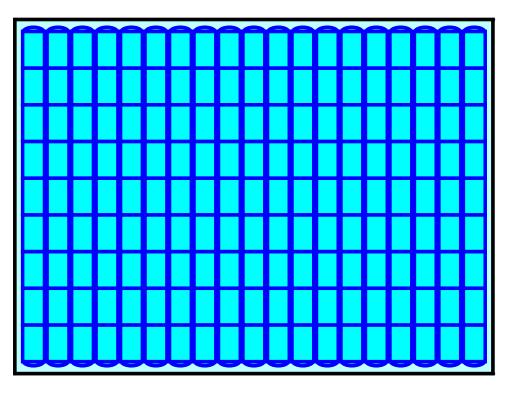
9 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 65.70' Row Length +18.0" End Stone x 2 = 68.70' Base Length 19 Rows x 51.0" Wide + 6.0" Spacing x 18 + 18.0" Side Stone x 2 = 92.75' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

171 Chambers x 45.9 cf = 7,855.7 cf Chamber Storage

22,300.7 cf Field - 7,855.7 cf Chambers = 14,444.9 cf Stone x 40.0% Voids = 5,778.0 cf Stone Storage

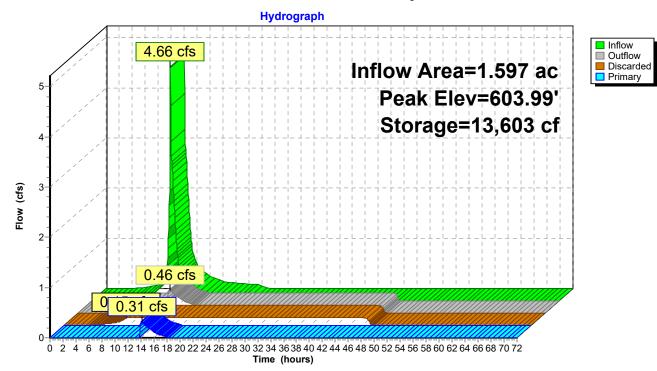
Chamber Storage + Stone Storage = 13,633.7 cf = 0.313 af Overall Storage Efficiency = 61.1% Overall System Size = 68.70' x 92.75' x 3.50'

171 Chambers 826.0 cy Field 535.0 cy Stone





Pond 3P: SC-740 Storm Tech System - Front



Summary for Pond 4P: CB

 Inflow Area =
 0.791 ac, 36.79% Impervious, Inflow Depth =
 3.31" for 25 YR event

 Inflow =
 1.51 cfs @
 12.56 hrs, Volume=
 0.218 af

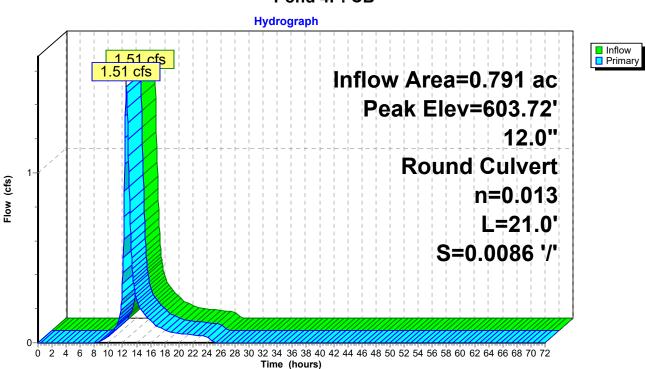
 Outflow =
 1.51 cfs @
 12.56 hrs, Volume=
 0.218 af, Atten= 0%, Lag= 0.0 min

 Primary =
 1.51 cfs @
 12.56 hrs, Volume=
 0.218 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 603.72' @ 12.56 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	602.93'	12.0" Round Culvert L= 21.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 602.93' / 602.75' S= 0.0086 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.51 cfs @ 12.56 hrs HW=603.72' (Free Discharge) —1=Culvert (Barrel Controls 1.51 cfs @ 3.13 fps)



Pond 4P: CB

Summary for Pond 5P: CB

 Inflow Area =
 0.806 ac, 57.63% Impervious, Inflow Depth = 4.77" for 25 YR event

 Inflow =
 4.18 cfs @ 12.09 hrs, Volume=
 0.320 af

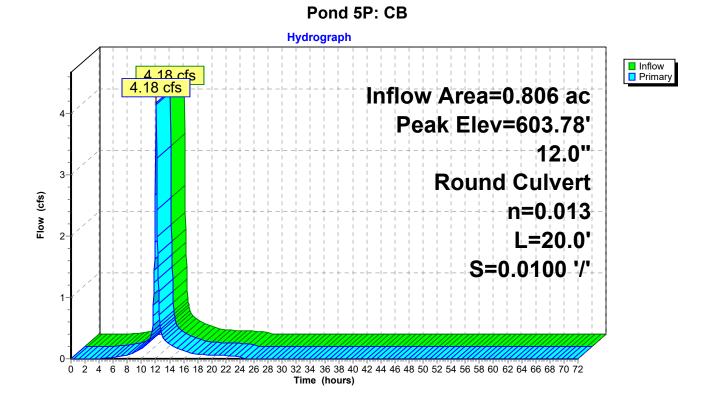
 Outflow =
 4.18 cfs @ 12.09 hrs, Volume=
 0.320 af, Atten= 0%, Lag= 0.0 min

 Primary =
 4.18 cfs @ 12.09 hrs, Volume=
 0.320 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 603.78' @ 12.09 hrs

H1 Drimony CO1 22 40 01 Downed Owleast	Device	e Routing	Invert	Outlet Devices
L= 20.0' Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 601.33' / 601.13' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf	#1	<u>U</u>		Inlet / Outlet Invert= 601.33' / 601.13' S= 0.0100 '/' Cc= 0.900

Primary OutFlow Max=4.07 cfs @ 12.09 hrs HW=603.69' (Free Discharge) -1=Culvert (Inlet Controls 4.07 cfs @ 5.18 fps)

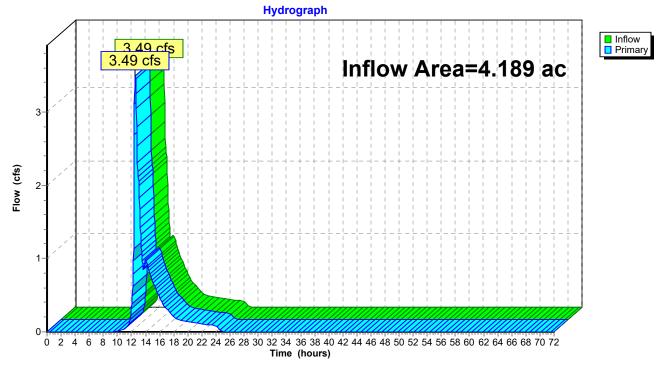


Summary for Link 1L: Town System

Inflow Area	a =	4.189 ac, 30.03% Impervious, Inflow Depth = 1.50" for 25 YR event
Inflow	=	3.49 cfs @ 12.53 hrs, Volume= 0.525 af
Primary	=	3.49 cfs $\overline{@}$ 12.53 hrs, Volume= 0.525 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 1L: Town System



Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method Page 66

Subcatchment1S: Rear Parking &	Runoff Area=72,157 sf 26.36% Impervious Runoff Depth=4.86" Flow Length=527' Tc=40.1 min CN=72 Runoff=4.64 cfs 0.671 af
Subcatchment 2S: Side Driveways &	Runoff Area=34,445 sf 36.79% Impervious Runoff Depth=5.45" Flow Length=527' Tc=40.1 min CN=77 Runoff=2.47 cfs 0.359 af
Subcatchment3S: Buildings, Southern	Runoff Area=35,108 sf 57.63% Impervious Runoff Depth=7.11" Tc=6.0 min CN=91 Runoff=6.08 cfs 0.478 af
Subcatchment4S: Access Driveways,	Runoff Area=40,758 sf 7.04% Impervious Runoff Depth=4.40" Flow Length=579' Tc=33.3 min CN=68 Runoff=2.59 cfs 0.343 af
	Rear Peak Elev=611.25' Storage=2,306 cf Inflow=4.64 cfs 0.671 af 3 cfs 0.086 af Primary=4.55 cfs 0.579 af Outflow=4.58 cfs 0.665 af
Pond 2P: CB 12.0" Rou	Peak Elev=612.20' Inflow=4.64 cfs 0.671 af ind Culvert n=0.013 L=95.0' S=0.0100 '/' Outflow=4.64 cfs 0.671 af
Pond 3P: SC-740 Storm Tech System - Discarded=0.15	Peak Elev=604.29' Storage=13,634 cf Inflow=6.93 cfs 0.837 af 5 cfs 0.524 af Primary=2.87 cfs 0.197 af Outflow=3.02 cfs 0.721 af
Pond 4P: CB 12.0" Rou	Peak Elev=604.11' Inflow=2.47 cfs 0.359 af Ind Culvert n=0.013 L=21.0' S=0.0086 '/' Outflow=2.47 cfs 0.359 af
Pond 5P: CB 12.0" Rou	Peak Elev=605.96' Inflow=6.08 cfs 0.478 af Ind Culvert n=0.013 L=20.0' S=0.0100 '/' Outflow=6.08 cfs 0.478 af
Link 1L: Town System	Inflow=9.88 cfs 1.119 af Primary=9.88 cfs 1.119 af

Summary for Subcatchment 1S: Rear Parking & Northern Abutters

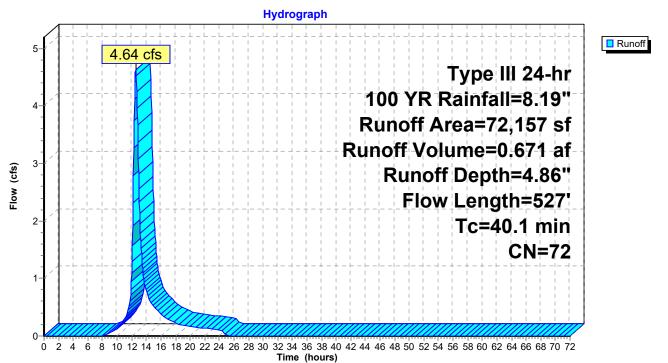
Runoff = 4.64 cfs @ 12.55 hrs, Volume= 0.671 af, Depth= 4.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YR Rainfall=8.19"

	А	rea (sf)	CN	Description		
*		13,899	98	Paved Roa	d HSB B	
		12,683	69	50-75% Gra	ass cover, F	Fair, HSG B
*		5,122	98	Buildings		
_		40,453	60	Woods, Fai	r, HSG B	
		72,157	72	Weighted A	verage	
53,136 73.64% Pervious Area					rvious Area	l
	19,021 26.36% Impervious Are					ea
	-		<u></u>		A	
	ŢĊ	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft	i) (ft/sec)	(cfs)	
	28.3	100	0.010	0.06		Sheet Flow, Sheet Flow
						Woods: Light underbrush n= 0.400 P2= 3.20"
	8.1	306	0.008	0 0.63		Shallow Concentrated Flow, Shallow Concentrated Flow
						Short Grass Pasture Kv= 7.0 fps
	3.7	121	0.0120	0 0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woo
_						Woodland Kv= 5.0 fps
	40 1	527	Total			

40.1 527 Total

Subcatchment 1S: Rear Parking & Northern Abutters



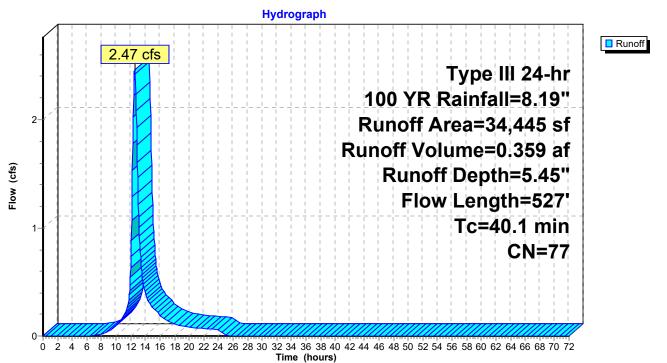
Summary for Subcatchment 2S: Side Driveways & Northern Abutters

Runoff = 2.47 cfs @ 12.54 hrs, Volume= 0.359 af, Depth= 5.45"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YR Rainfall=8.19"

	A	rea (sf)	CN	Description						
*		7,619	98	Paved Road	Paved Road HSB B					
		12,149	69	50-75% Gra	ass cover, F	Fair, HSG B				
*		5,055	98	Buildings						
_		9,622	60	Woods, Fai	r, HSG B					
		34,445	77	Weighted A	verage					
		21,771		63.21% Per	vious Area					
	12,674 36.79% Impervious Are					ea				
	Тс	Length	Slope	e Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow				
						Woods: Light underbrush n= 0.400 P2= 3.20"				
	8.1	306	0.0080	0.63		Shallow Concentrated Flow, Shallow Concentrated Flow				
						Short Grass Pasture Kv= 7.0 fps				
	3.7	121	0.0120	0.55		Shallow Concentrated Flow, Shallow Concetrate Flow - Woods				
_						Woodland Kv= 5.0 fps				
	40.1	527	Total							

Subcatchment 2S: Side Driveways & Northern Abutters

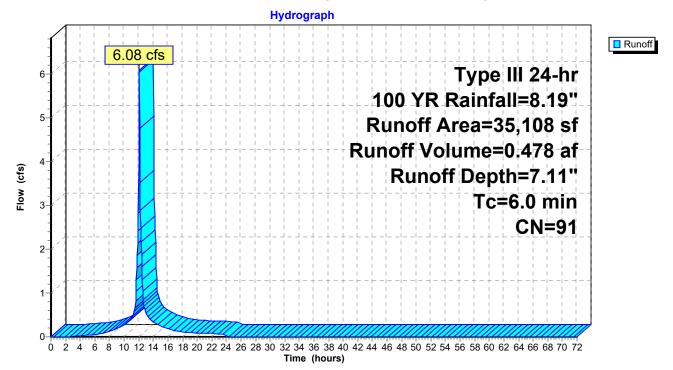


Runoff = 6.08 cfs @ 12.09 hrs, Volume= 0.478 af, Depth= 7.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YR Rainfall=8.19"

	A	rea (sf)	CN	Description							
*		10,966	98	Paved Road HSB B							
		3,289	69	50-75% Grass cover, Fair, HSG B							
*		9,267	98	Buildings							
		11,586	85	Gravel roads, HSG B							
		35,108	91	Weighted A	verage						
		14,875		42.37% Pervious Area							
		20,233		57.63% Impervious Area							
	Тс	Length	Slope		Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	6.0					Direct Entry, Direct Entry					





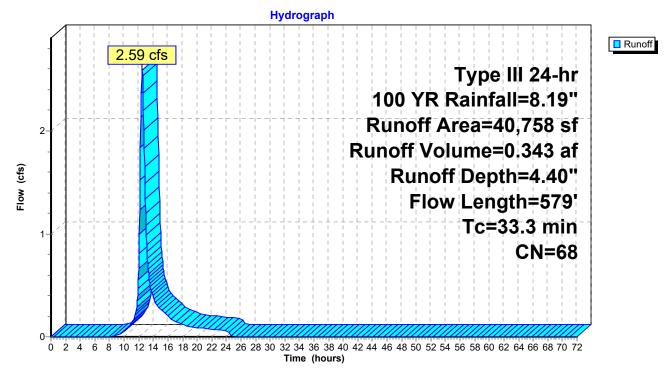
Summary for Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods

Runoff = 2.59 cfs @ 12.47 hrs, Volume= 0.343 af, Depth= 4.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YR Rainfall=8.19"

	A	rea (sf)	CN E	Description		
*		2,870	98 F	Paved Roa	d HSB B	
		26,302	69 5	50-75% Gra	ass cover, F	Fair, HSG B
*		0		Buildings		
_		11,586	60 V	Voods, Fai	r, HSG B	
		40,758	68 V	Veighted A	verage	
		37,888	g	92.96% Pei	vious Area	
		2,870	7	7.04% Impe	ervious Area	a
	-				O	
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.3	100	0.0100	0.06		Sheet Flow, Sheet Flow
						Woods: Light underbrush n= 0.400 P2= 3.20"
	4.3	214	0.0140	0.83		Shallow Concentrated Flow, Shallow Concentrated Flow
		400		~~~~	04	Short Grass Pasture Kv= 7.0 fps
	0.1	100	0.1100	23.09	577.34	Channel Flow, Channel
						Area= 25.0 sf Perim= 15.0' r= 1.67'
	0.6	165	0 0060	4 65	195 00	n= 0.030 Earth, grassed & winding
	0.6	165	0.0060	4.65	185.92	Channel Flow, Drain Channel Area= 40.0 sf Perim= 30.0' r= 1.33'
						n = 0.030 Earth, grassed & winding
_		570	Tatal			n- 0.000 Latin, grassed & winding
	33.3	579	Total			

Subcatchment 4S: Access Driveways, Southern Lawn, & Eastern Woods



Summary for Pond 1P: SC-740 Storm Tech System - Rear

Inflow Area =	1.656 ac, 26.36% Impervious, Inflow De	epth = 4.86" for 100 YR event
Inflow =	4.64 cfs @ 12.55 hrs, Volume=	0.671 af
Outflow =	4.58 cfs @ 12.55 hrs, Volume=	0.665 af, Atten= 1%, Lag= 0.0 min
Discarded =	0.03 cfs @ 8.75 hrs, Volume=	0.086 af
Primary =	4.55 cfs @ 12.55 hrs, Volume=	0.579 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 611.25' @ 12.55 hrs Surf.Area= 1,096 sf Storage= 2,306 cf

Plug-Flow detention time= 124.9 min calculated for 0.665 af (99% of inflow) Center-of-Mass det. time= 119.3 min (970.5 - 851.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	607.50'	1,020 cf	20.50'W x 53.46'L x 3.50'H Field A
			3,836 cf Overall - 1,286 cf Embedded = 2,549 cf x 40.0% Voids
#2A	608.00'	1,286 cf	ADS_StormTech SC-740 +Cap x 28 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			4 Rows of 7 Chambers
		2 306 cf	Total Available Storage

2,306 cf Total Available Storage

Storage Group A created with Chamber Wizard

Routing	Invert	Outlet Devices
Discarded	607.50'	1.020 in/hr Exfiltration over Surface area
Primary	610.75'	5.0' long x 5.0' breadth Broad-Crested Rectangular Weir
		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
		2.50 3.00 3.50 4.00 4.50 5.00 5.50
		Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65
		2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88
	Discarded	Discarded 607.50'

Discarded OutFlow Max=0.03 cfs @ 8.75 hrs HW=607.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=4.55 cfs @ 12.55 hrs HW=611.25' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 4.55 cfs @ 1.83 fps)

Pond 1P: SC-740 Storm Tech System - Rear - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

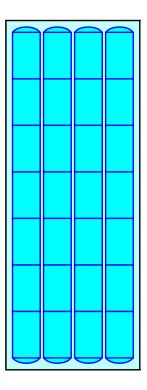
7 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 51.46' Row Length +12.0" End Stone x 2 = 53.46' Base Length 4 Rows x 51.0" Wide + 6.0" Spacing x 3 + 12.0" Side Stone x 2 = 20.50' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

28 Chambers x 45.9 cf = 1,286.3 cf Chamber Storage

3,835.5 cf Field - 1,286.3 cf Chambers = 2,549.2 cf Stone x 40.0% Voids = 1,019.7 cf Stone Storage

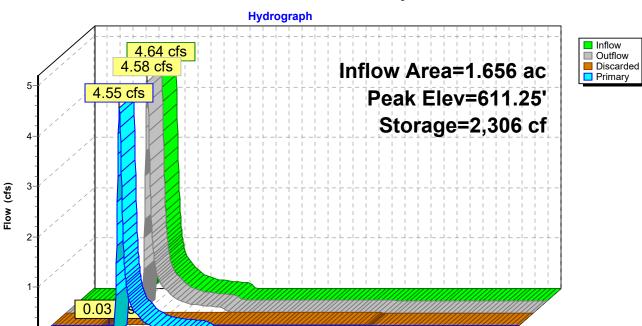
Chamber Storage + Stone Storage = 2,306.0 cf = 0.053 afOverall Storage Efficiency = 60.1%Overall System Size = $53.46' \times 20.50' \times 3.50'$

28 Chambers 142.1 cy Field 94.4 cy Stone





0



0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

Pond 1P: SC-740 Storm Tech System - Rear

Summary for Pond 2P: CB

 Inflow Area =
 1.656 ac, 26.36% Impervious, Inflow Depth = 4.86" for 100 YR event

 Inflow =
 4.64 cfs @ 12.55 hrs, Volume=
 0.671 af

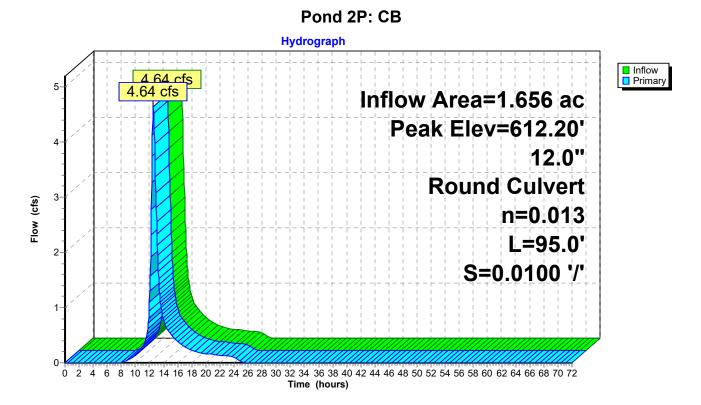
 Outflow =
 4.64 cfs @ 12.55 hrs, Volume=
 0.671 af, Atten= 0%, Lag= 0.0 min

 Primary =
 4.64 cfs @ 12.55 hrs, Volume=
 0.671 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 612.20' @ 12.55 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	609.29'	12.0" Round Culvert L= 95.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 609.29' / 608.34' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=4.63 cfs @ 12.55 hrs HW=612.20' (Free Discharge)



Summary for Pond 3P: SC-740 Storm Tech System - Front

Inflow Area =	1.597 ac, 47.31% Impervious, Inflow De	epth = 6.29" for 100 YR event
Inflow =	6.93 cfs @ 12.09 hrs, Volume=	0.837 af
Outflow =	3.02 cfs @ 12.47 hrs, Volume=	0.721 af, Atten= 56%, Lag= 22.8 min
Discarded =	0.15 cfs @ 8.40 hrs, Volume=	0.524 af
Primary =	2.87 cfs @ 12.47 hrs, Volume=	0.197 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 604.29' @ 12.47 hrs Surf.Area= 6,372 sf Storage= 13,634 cf

Plug-Flow detention time= 693.5 min calculated for 0.721 af (86% of inflow) Center-of-Mass det. time= 632.1 min (1,433.4 - 801.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	600.50'	5,778 cf	92.75'W x 68.70'L x 3.50'H Field A
			22,301 cf Overall - 7,856 cf Embedded = 14,445 cf x 40.0% Voids
#2A	601.00'	7,856 cf	ADS_StormTech SC-740 +Cap x 171 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			19 Rows of 9 Chambers
		13 634 cf	Total Available Storage

13,634 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	600.50'	1.020 in/hr Exfiltration over Surface area
#2	Primary	603.90'	5.0' long x 5.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88

Discarded OutFlow Max=0.15 cfs @ 8.40 hrs HW=600.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.15 cfs)

Primary OutFlow Max=2.54 cfs @ 12.47 hrs HW=604.25' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 2.54 cfs @ 1.45 fps)

Pond 3P: SC-740 Storm Tech System - Front - Chamber Wizard Field A

Chamber Model = ADS_StormTechSC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

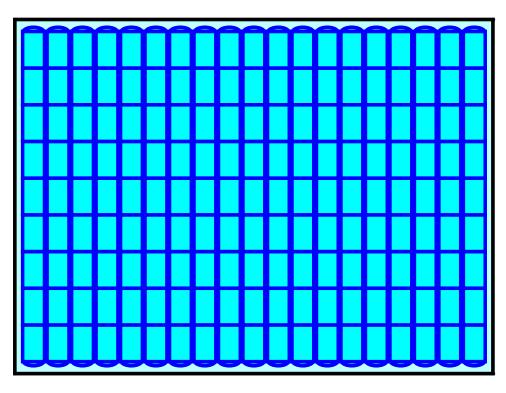
9 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 65.70' Row Length +18.0" End Stone x 2 = 68.70' Base Length 19 Rows x 51.0" Wide + 6.0" Spacing x 18 + 18.0" Side Stone x 2 = 92.75' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

171 Chambers x 45.9 cf = 7,855.7 cf Chamber Storage

22,300.7 cf Field - 7,855.7 cf Chambers = 14,444.9 cf Stone x 40.0% Voids = 5,778.0 cf Stone Storage

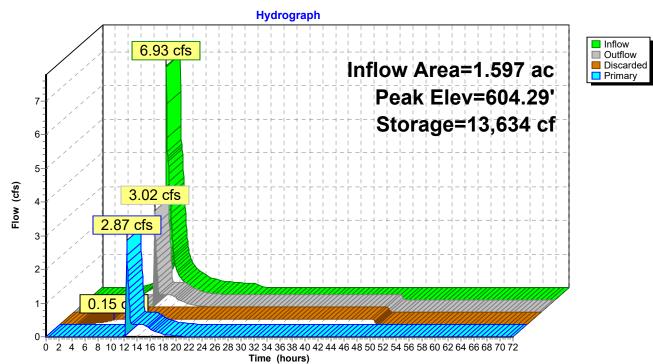
Chamber Storage + Stone Storage = 13,633.7 cf = 0.313 af Overall Storage Efficiency = 61.1% Overall System Size = 68.70' x 92.75' x 3.50'

171 Chambers 826.0 cy Field 535.0 cy Stone









Summary for Pond 4P: CB

 Inflow Area =
 0.791 ac, 36.79% Impervious, Inflow Depth =
 5.45" for 100 YR event

 Inflow =
 2.47 cfs @
 12.54 hrs, Volume=
 0.359 af

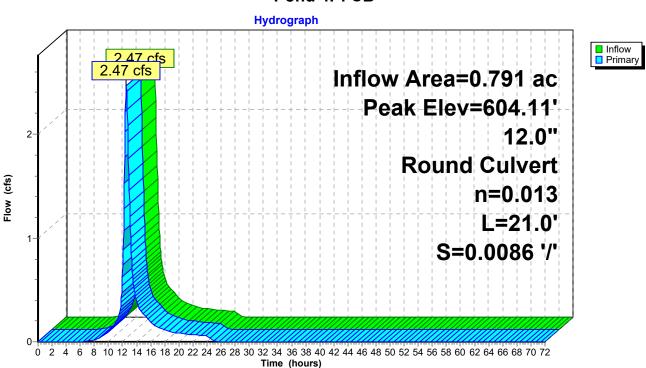
 Outflow =
 2.47 cfs @
 12.54 hrs, Volume=
 0.359 af, Atten= 0%, Lag= 0.0 min

 Primary =
 2.47 cfs @
 12.54 hrs, Volume=
 0.359 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 604.11' @ 12.54 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	602.93'	12.0" Round Culvert L= 21.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 602.93' / 602.75' S= 0.0086 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.46 cfs @ 12.54 hrs HW=604.11' (Free Discharge)



Pond 4P: CB

Summary for Pond 5P: CB

 Inflow Area =
 0.806 ac, 57.63% Impervious, Inflow Depth = 7.11" for 100 YR event

 Inflow =
 6.08 cfs @ 12.09 hrs, Volume=
 0.478 af

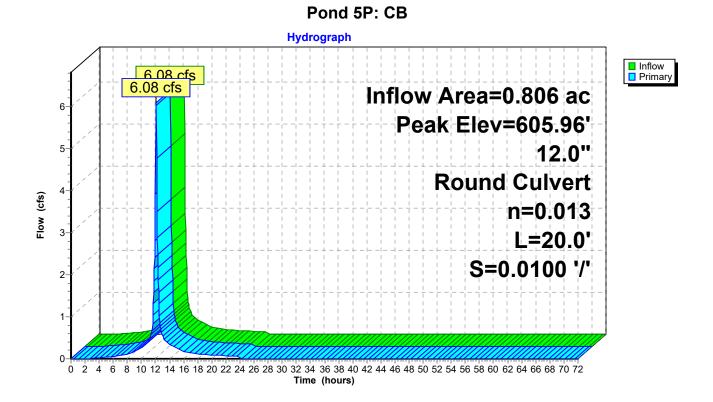
 Outflow =
 6.08 cfs @ 12.09 hrs, Volume=
 0.478 af, Atten= 0%, Lag= 0.0 min

 Primary =
 6.08 cfs @ 12.09 hrs, Volume=
 0.478 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 605.96' @ 12.09 hrs

Device Routin	ng Invert	Outlet Devices
#1 Prima	0	12.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 601.33' / 601.13' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=5.92 cfs @ 12.09 hrs HW=605.77' (Free Discharge) -1=Culvert (Inlet Controls 5.92 cfs @ 7.54 fps)



Summary for Link 1L: Town System

Inflow Area	a =	4.189 ac, 30.03% Impervious, Inflow Depth = 3.21" for 100 YR event	
Inflow	=	9.88 cfs @ 12.47 hrs, Volume= 1.119 af	
Primary	=	9.88 cfs $\overline{@}$ 12.47 hrs, Volume= 1.119 af, Atten= 0%, Lag= 0.0 min	

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 1L: Town System

